

RECENT MÖSSBAUER STUDIES ON MFe_2O_4 AND $M_xN_{1-x}Fe_2O_4$ FERRITES, WITH M, N = Ni, Zn, Mg



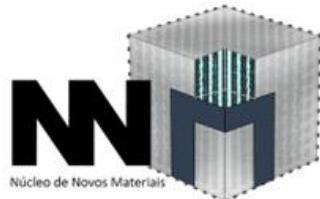
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XVII Latin American Conference On The Applications Of The Mössbauer Effect

LACAME'22



CONTENT

1. Ferrites with spinel structure

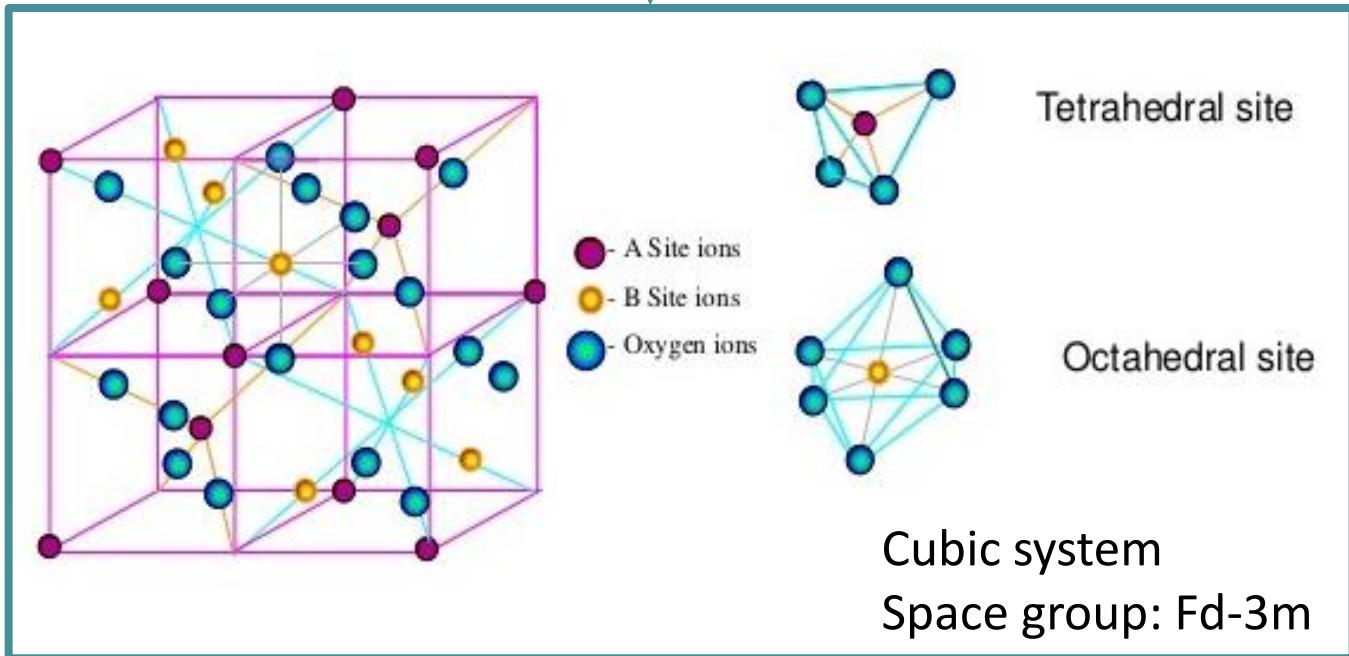
2. Recoilless *f*-factor for MFe₂O₄; M = Fe, Ni, Mg

3. Ni_{1-x}Zn_xFe₂O₄

4. Mg_{1-x}Zn_xFe₂O₄

1. FERRITES WITH SPINEL STRUCTURE

Spinel structure



Chemical formula



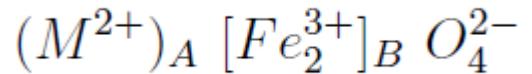
M are chemical elements with oxidation state +2



λ : inversion degree $0 \leq \lambda \leq 1$
(): tetrahedral sites (A-sites)
[]: octahedral sites [B-sites]

Classification of spinel structure

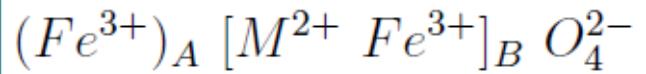
Normal Spinel



Divalent cations M^{2+} occupy tetrahedral sites, trivalent cations Fe^{3+} occupy octahedral sites.

$$\lambda = 0$$

Inverse Spinel



Divalent cations M^{2+} occupy octahedral sites, trivalent cations Fe^{3+} occupy tetrahedral and octahedral sites.

$$\lambda = 1$$

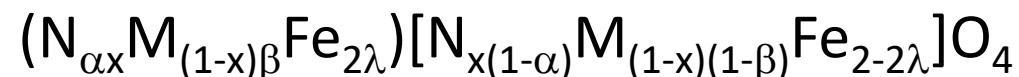
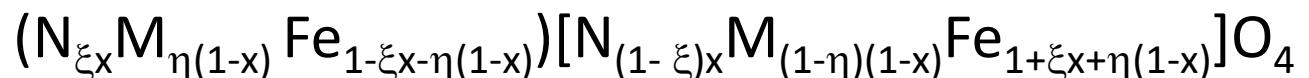
Mixed Spinel



M^{2+} and Fe^{3+} occupy tetrahedral and octahedral sites simultaneously and in different proportions.

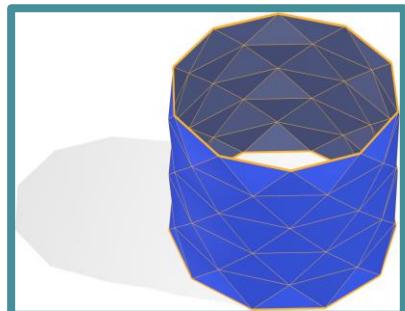
$$0 < \lambda < 1$$

Quaternary ferrites



Properties

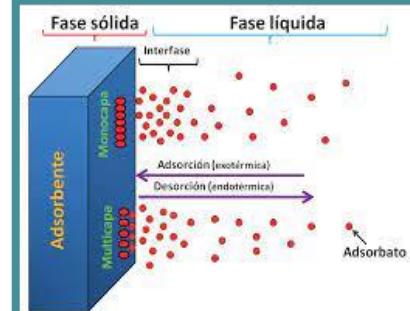
Superficial area



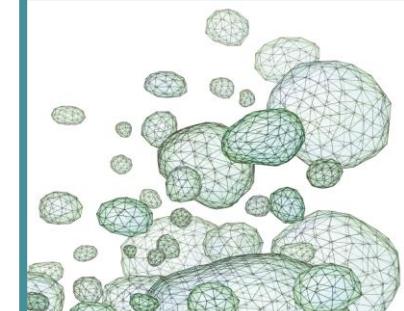
Reactivity



Reversible adsorption



Particle size



Magnetic separation



2. RECOILLESS *f*-FACTOR for MFe₂O₄; M = Fe, Ni, Mg

The **recoilless *f*-factor** is the fraction of gamma rays which are emitted and absorbed without recoil.

$$\longrightarrow f = e^{-k^2 \langle x^2 \rangle}$$

Debye model for lattice vibrations

$$f = \exp \left\{ - \left(\frac{3E_R}{2k_B \theta_D} \right) \left[1 + \left(\frac{2T}{\theta_D} \right)^2 \int_0^{\theta_D/T} \frac{x}{e^x - 1} dx \right] \right\}$$

The recoilless *f*-factor is closely related with the atomic vibrations in the solid in which the Mössbauer nucleus is embedded and allows determination of relative atomic, molecular or weight fractions of iron compounds in the absorber.

Subspectral area ratio method

For uniform and nonpolarizing absorbers (Transmission Integral):

$$N(E) = BG + \eta_M f_s \frac{2}{\pi \Gamma_0} \int_{-\infty}^{+\infty} d\psi \frac{\Gamma_0^2/4}{(\psi + E)^2 + \Gamma_0^2/4} (e^{-\sigma'_a \psi} - 1)$$

where $\sigma'_a(E) = \sum_i f_{a,i} n_{a,i} \sigma_{a,i}(E)$

In the thin absorber approximation:

$$N_{th}(E) = BG - \eta_M f_s \frac{2}{\pi \Gamma_0} \sum_i f_{a,i} n_{a,i} \int_{-\infty}^{+\infty} d\psi \frac{\Gamma_0^2/4}{(\psi + E)^2 + \Gamma_0^2/4} \sigma_{a,i} \psi$$

The total spectral area is given by:

$$A_T = \int_{-\infty}^{+\infty} dE [BG - N_{th}(E)] = \sum_i \frac{\pi}{2} \sigma_0 \Gamma_0 \eta_M f_s f_{a,i} n_{a,i}$$

Subspectral area ratio method

$$A_T = \sum_i A_i = \sum_i \frac{\pi}{2} \sigma_0 \Gamma_0 \eta_M f_s f_{a,i} n_{a,i}$$

Absorber made of homogeneous mixture of compound, i , and reference, r :

$$\frac{A_i}{A_r} = \frac{\frac{\pi}{2} \sigma_0 \Gamma_0 \eta_M f_s f_{a,i} n_{a,i}}{\frac{\pi}{2} \sigma_0 \Gamma_0 \eta_M f_s f_{a,r} n_{a,r}} = \frac{f_{a,i} n_{a,i}}{f_{a,r} n_{a,r}}$$

$$n_{a,j} = \frac{N_A m_{a,j} a O_{a,j} N_{a,j}}{\mu_{a,j} A}$$

ONE relative f -factor 

σ_0 : cross-section at resonance

Γ_0 : FWHM of Mössbauer transition

η_M : Mössbauer gamma of BG
 f : recoilless f -factor

n : total number of ^{57}Fe per cm^2 .

N_A : Avogadro number

m : mass

a : ^{57}Fe natural abundance

O : iron occupancy factor

N : number of Fe per formula unit

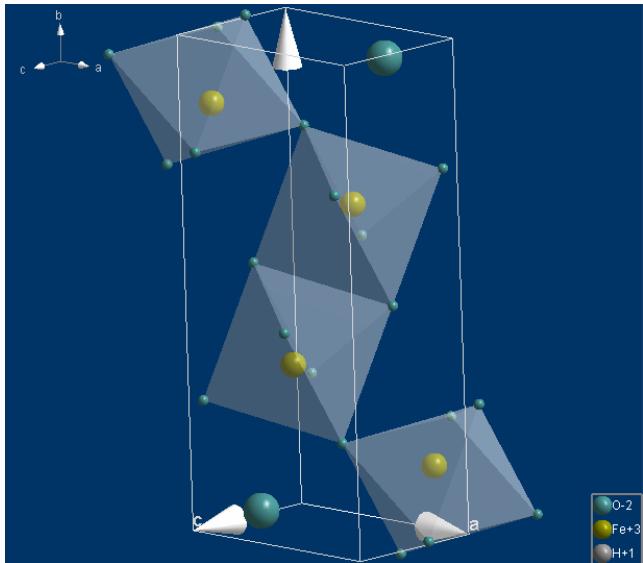
μ : molar weight

A : spectral área

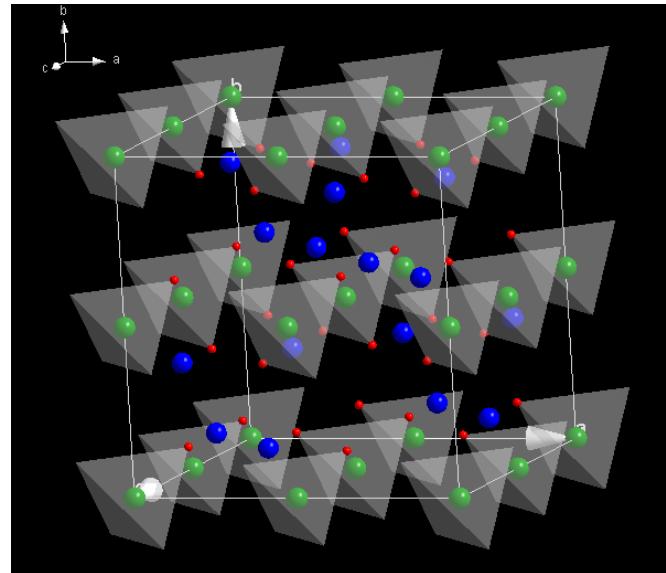
$$\frac{f_i}{f_r} = \left(\frac{m_r}{m_i} \right) \left(\frac{\mu_i}{\mu_r} \right) \left(\frac{A_i}{A_r} \right)$$

Extension of the area ratio method

The subspectral area ratio method at a single T assumes that there is only ONE average f -factor value for irons at all sites in the compound. Therefore, we will call this method the **One relative f -factor**.



Fe^{3+} at one crystallographic site



Fe^{3+} at two crystallographic sites

Is it possible to extend this subspectral area method to determine simultaneously **TWO relative f -factors**, associated to two iron sites in the compound?

Extension of the area ratio method

Total spectral area

$$A_T = A_1 + A_2 + A_r$$

$$\frac{A_1}{A_r} + \frac{A_2}{A_r} = \frac{A_T}{A_r} - 1$$

Spectral area of site i .

$$A_i = \frac{\pi}{2} \sigma_0 \Gamma_0 n_M f_s f_{a,i} n_{a,i}$$

Combination of previous equations

$$\frac{n_1 f_1}{n_r f_r} + \frac{n_2 f_2}{n_r f_r} = \frac{A_T}{A_r} - 1$$

Sum of $^{57}\text{Fe}/\text{cm}^2$ thicknesses of two Fe sites

$$n_1 + n_2 = n_{\text{compound}}$$

fraction y (or $1-y$) of Fe atoms in the compound are located in site 1 (or 2).

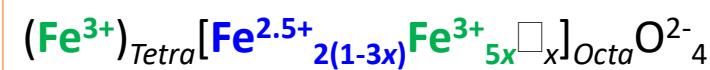
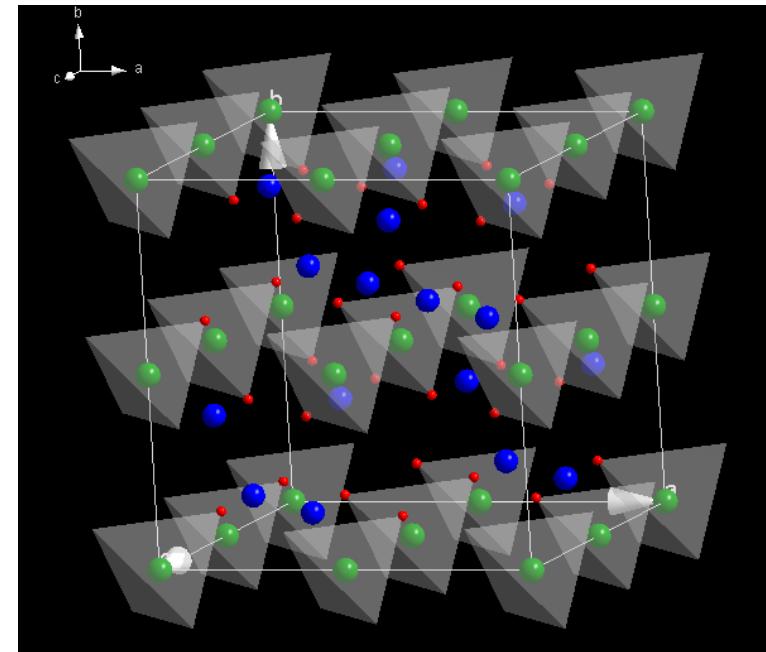
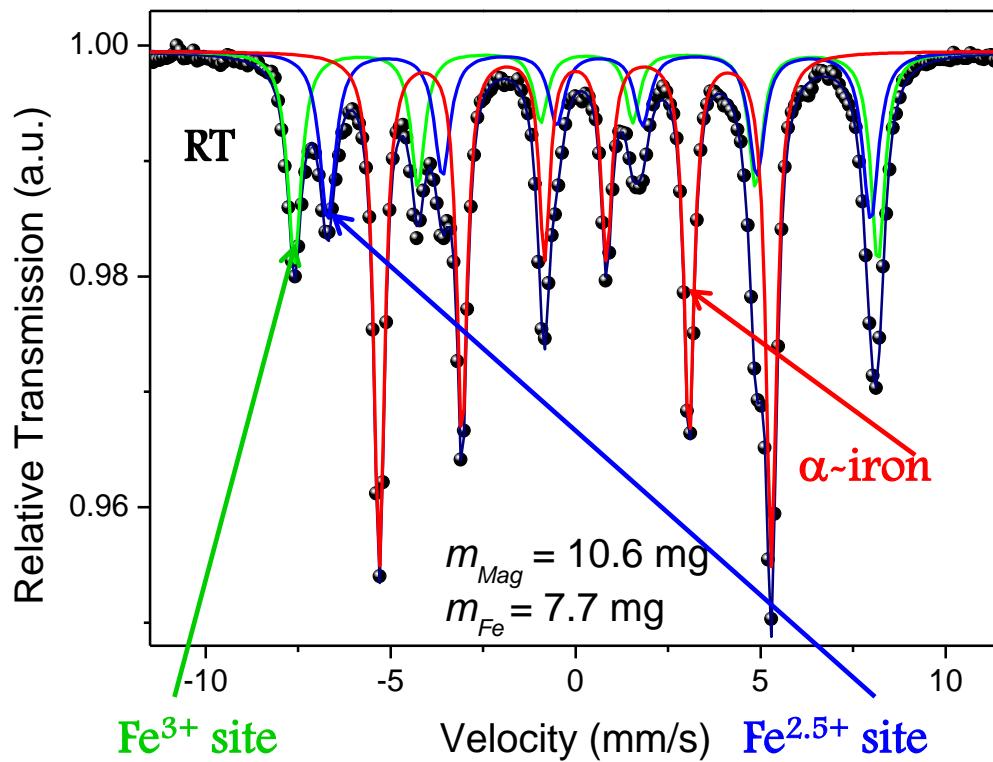
$$n_1 = y n_{\text{compound}} \quad n_2 = (1-y) n_{\text{compound}}$$

$^{57}\text{Fe}/\text{cm}^2$ thicknesses of a compound.

$$n_{\text{compound}} = \frac{N_A m_{\text{compound}} a O_{\text{compound}} N_{\text{compound}}}{\mu_{\text{compound}} A}$$

Magnetite

Mixture of magnetite ($\text{Fe}_{3-x}\text{O}_4$) and iron powder



$$\frac{f_{\text{Fe}^{3+}}}{f_{\text{Fe}}} = \left(\frac{1}{1+5x} \right) \left(\frac{\mu_{\text{Mag}}}{\mu_{\text{Fe}}} \right) \left(\frac{m_{\text{Fe}}}{m_{\text{Mag}}} \right) \left(\frac{\frac{A_T}{A_{\text{Fe}}} - 1}{\frac{A_{\text{Fe}^{2.5+}}}{A_{\text{Fe}^{3+}}} + 1} \right)$$

$$\frac{f_{\text{Fe}^{2.5+}}}{f_{\text{Fe}}} = \left(\frac{1}{2-6x} \right) \left(\frac{\mu_{\text{Mag}}}{\mu_{\text{Fe}}} \right) \left(\frac{m_{\text{Fe}}}{m_{\text{Mag}}} \right) \left(\frac{\frac{A_T}{A_{\text{Fe}}} - 1}{\frac{A_{\text{Fe}^{3+}}}{A_{\text{Fe}^{2.5+}}} + 1} \right)$$

Masses of magnetite (m_{Mag}) and iron powder (m_{Fe}). Relative spectral areas $A_{Fe^{3+}}$, $A_{Fe^{2.5+}}$, A_{Fe} and f -factors $f_{Fe^{3+}}$, $f_{Fe^{2.5+}}$, f_{Fe} for Fe^{3+} and $Fe^{2.5+}$ sites of magnetite and iron powder, respectively. [$m_{Thin} < m_{Mag}$, $m_{Fe} < m_{Ideal}$].

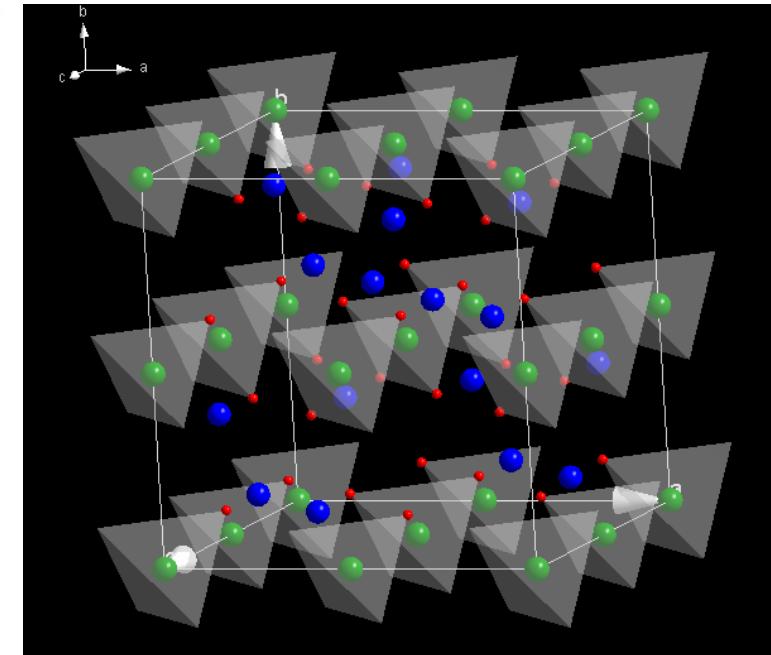
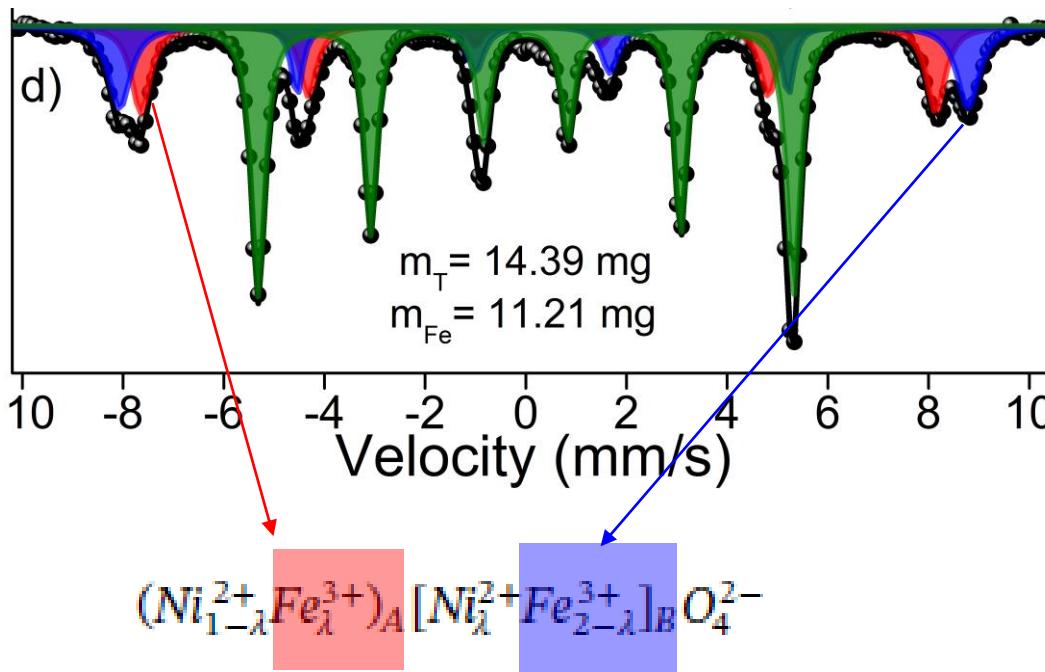
m_{Mag} (mg)	m_{Fe} (mg)	A_{Fe}	$A_{Fe^{3+}}$	$A_{Fe^{2.5+}}$	$f_{Fe^{3+}}/f_{Fe}$	$f_{Fe^{2.5+}}/f_{Fe}$
5.9	4.4	54.8	22.1	23.1	0.90	0.85
7.1	5.2	53.0	22.4	24.6	0.95	0.90
8.8	6.4	51.0	23.4	25.6	1.02	0.96
13.6	9.9	51.7	23.5	24.8	0.99	0.94

$$f_{Fe^{3+}}/f_{Fe} = 0.97 \pm 0.05, f_{Fe^{2.5+}}/f_{Fe} = 0.92 \pm 0.05; \text{ and } f_{Fe^{2.5+}}/f_{Fe^{3+}} = 0.95 \pm 0.05$$

$$f_{Fe^{2.5+}}/f_{Fe^{3+}} = 0.94 \pm 0.02 \text{ reported by Sawatzky et al., Phys. Rev. 183 (1969) 383 .}$$

Nickel ferrite

Mixture of NiFe_2O_4 and iron powder



$$\frac{f_{Fe_A^{3+}}}{f_{Fe}} = \left(\frac{1}{\lambda}\right) \left(\frac{m_{Fe}}{m_T}\right) \left(\frac{\mu_T}{\mu_{Fe}}\right) \frac{\left(\frac{A_M}{A_{Fe}} - 1\right)}{\left(\frac{A_{Fe_B^{3+}}}{A_{Fe_A^{3+}}} + 1\right)}$$

$$\frac{f_{Fe_B^{3+}}}{f_{Fe}} = \left(\frac{1}{2-\lambda}\right) \left(\frac{m_{Fe}}{m_T}\right) \left(\frac{\mu_T}{\mu_{Fe}}\right) \frac{\left(\frac{A_M}{A_{Fe}} - 1\right)}{\left(\frac{A_{Fe_A^{3+}}}{A_{Fe_B^{3+}}} + 1\right)}$$

Lagarec, Rancourt, Recoil: Mössbauer Spectral Analysis Software for Windows, version 1.0 (University of Ottawa, Canada, 1998).

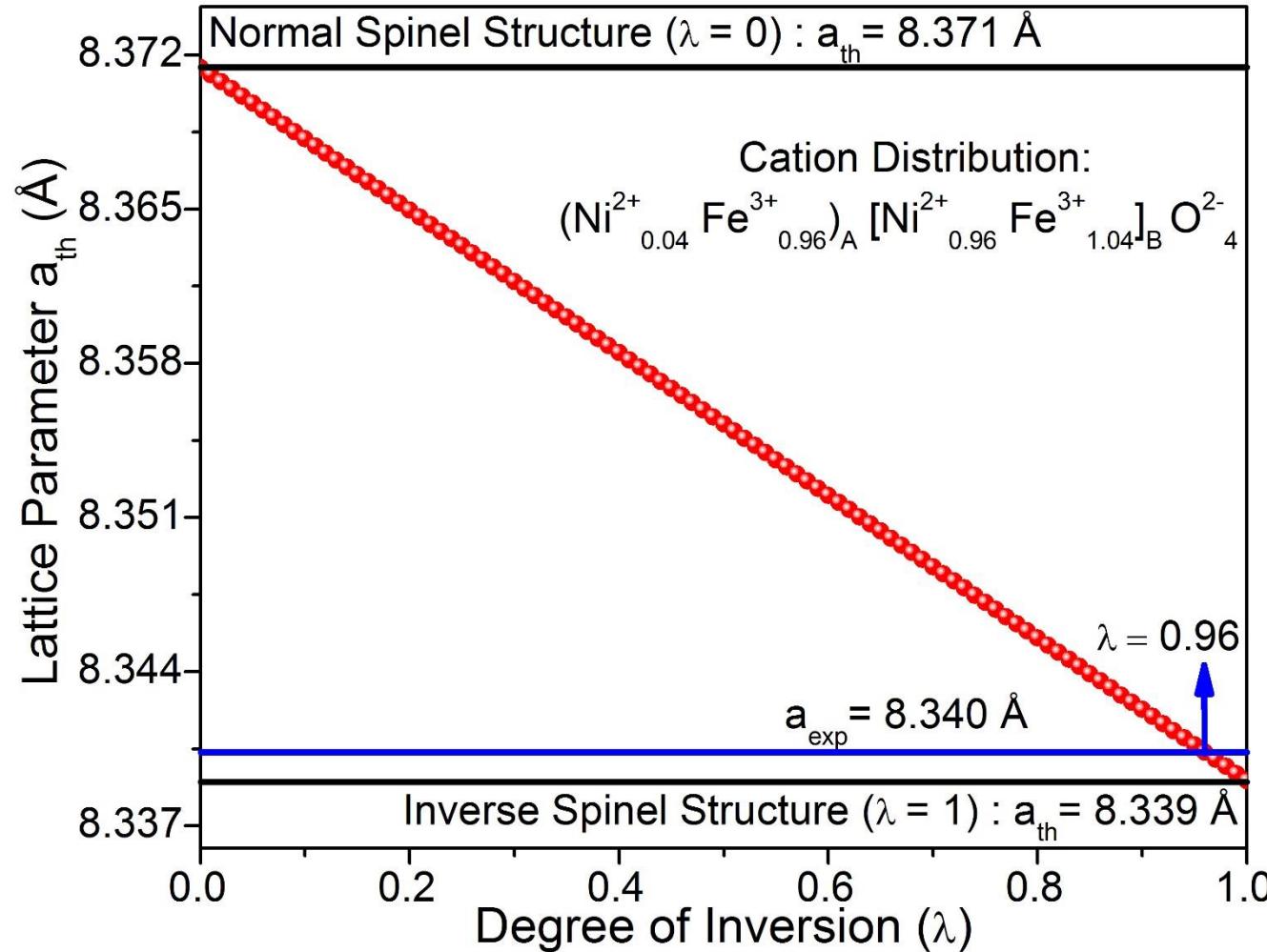
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Determination of degree of inversion

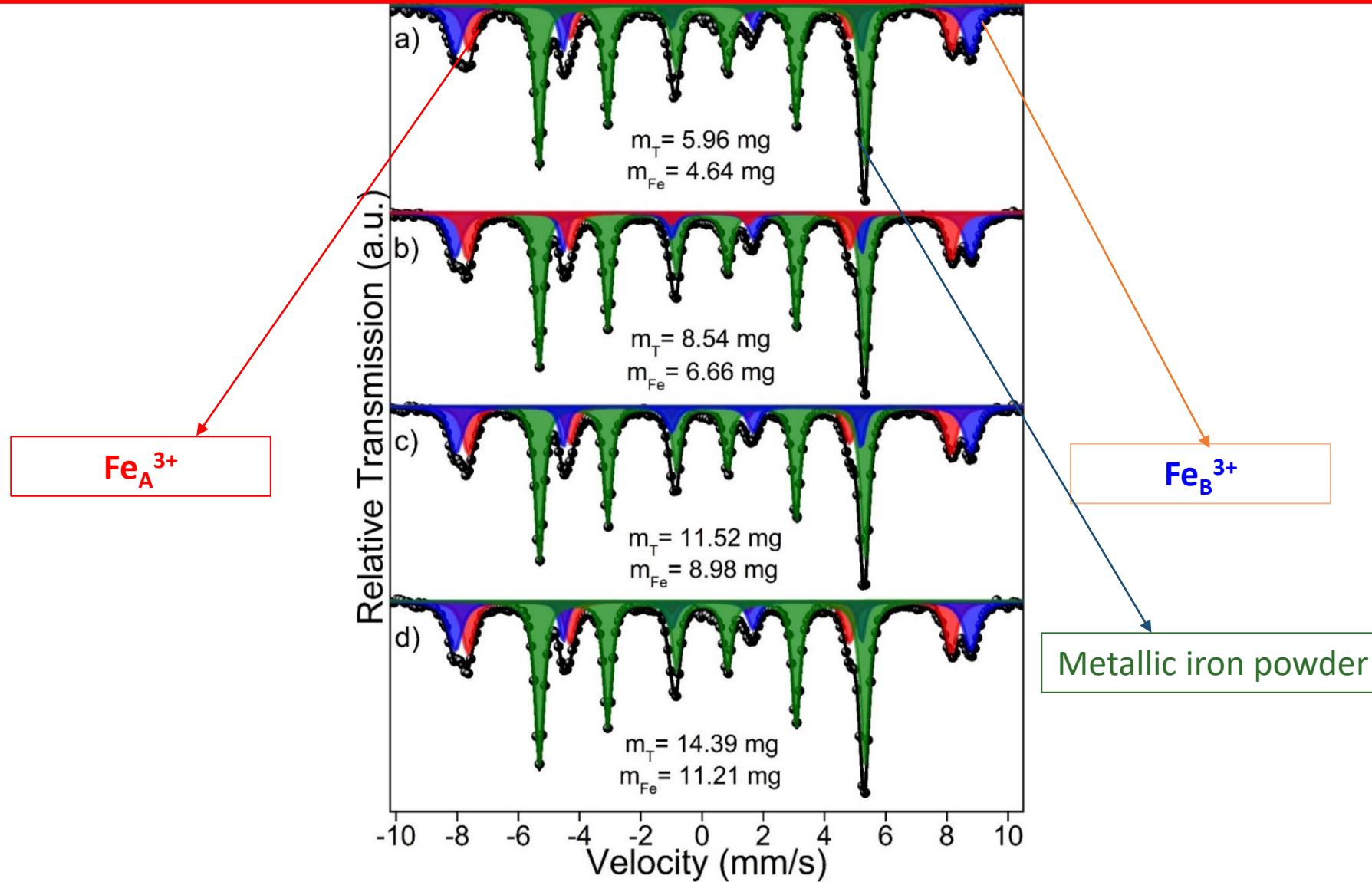
$$a_{th} = \frac{8}{3\sqrt{3}} [(r_A + R_0) + \sqrt{3}(r_B + R_0)]$$

$$r_A = ((1-\lambda)r_{Ni^{2+}} + \lambda r_{Fe^{3+}})$$

$$r_B = \frac{1}{3}[\lambda r_{Ni^{2+}} + (2-\lambda)r_{Fe^{3+}}]$$



300 K thickness-corrected Mössbauer spectra of the homogeneous mixtures of NiFe_2O_4 and metallic iron powder. The masses are indicated in each spectrum.



Lagarec, Rancourt, Recoil: Mössbauer Spectral Analysis Software for Windows, version 1.0 (University of Ottawa, Canada, 1998).

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Masses of the NiFe_2O_4 (m_T) and metallic Fe (m_{Fe}) materials used in the Mössbauer absorbers.

Sample code	m_T (mg)	m_{Fe} (mg)
a)	5.96	4.64
b)	8.54	6.66
c)	11.52	8.98
d)	14.39	11.21

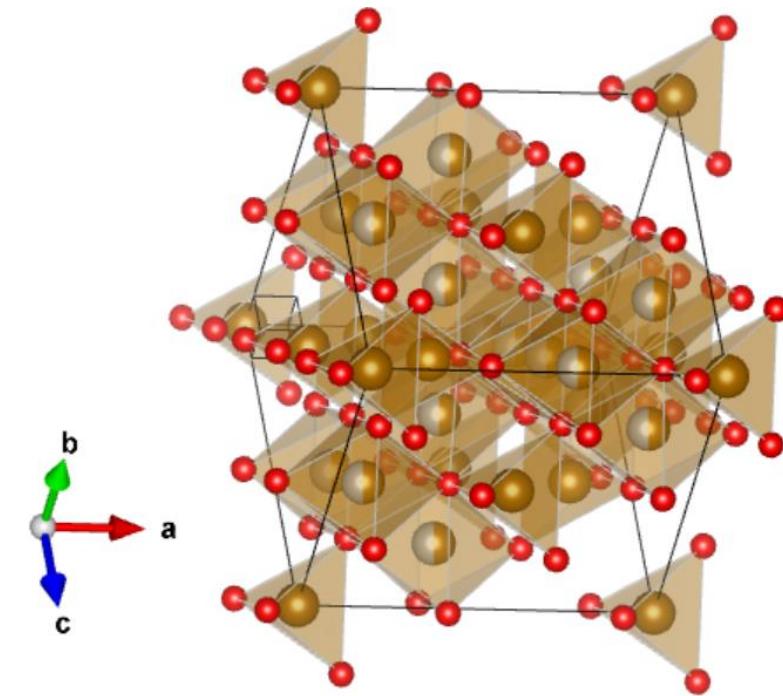
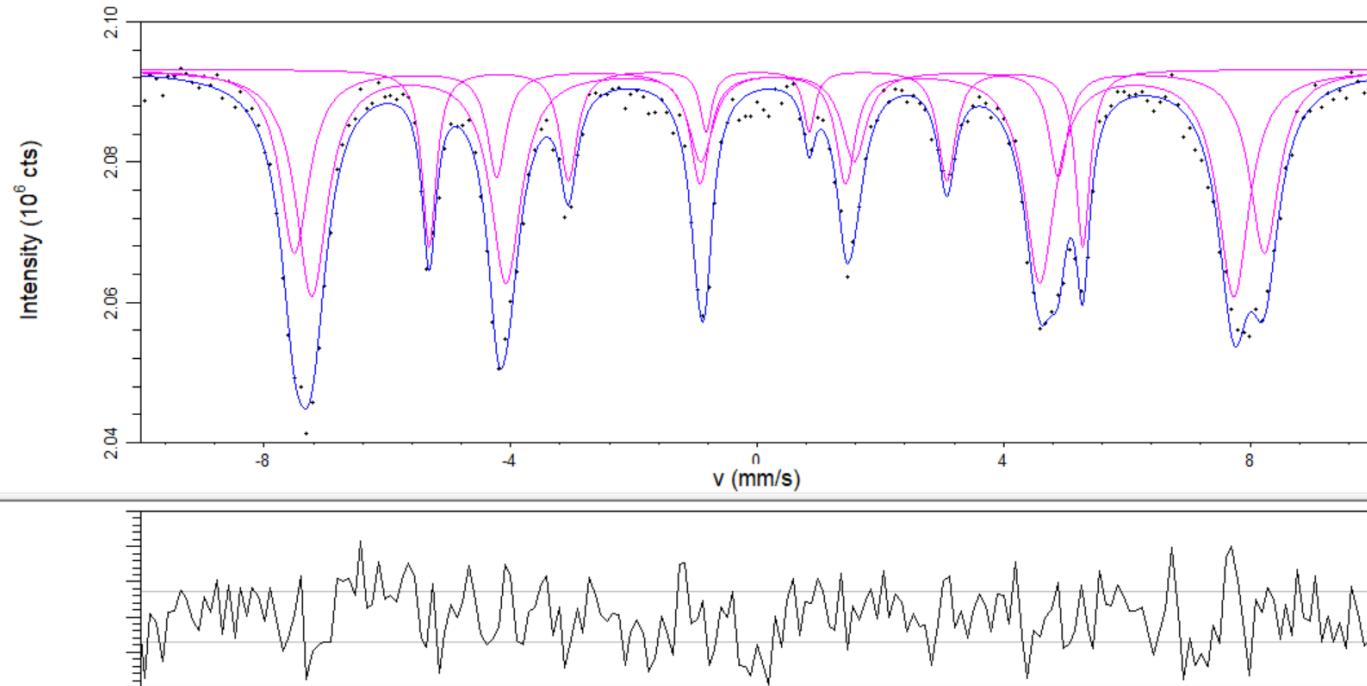
Spectral areas and Mössbauer recoilless f -factors of the (A) and [B] sites of NiFe_2O_4 . A_{Fe} and f_{Fe} are the spectral area and the Mössbauer recoilless f -factor of the metallic Fe powder.

Sample	$A_{Fe_A^{3+}}$	$A_{Fe_B^{3+}}$	A_{Fe}	$\frac{f_{Fe_A^{3+}}}{f_{Fe}}$	$\frac{f_{Fe_B^{3+}}}{f_{Fe}}$	$f_{Fe_A^{3+}}$	$f_{Fe_B^{3+}}$	$\frac{f_{Fe_B^{3+}}}{f_{Fe_A^{3+}}}$
a)	20.1	23.7	56.2	1.22	1.33	0.85	0.93	1.09
b)	20.0	23.4	56.6	1.20	1.30	0.84	0.91	1.08
c)	19.9	23.7	56.4	1.20	1.32	0.84	0.93	1.10
d)	20.1	23.6	56.3	1.22	1.32	0.85	0.92	1.08

$$\frac{f_{Fe_B^{3+}}}{f_{Fe_A^{3+}}} = 1.09 \pm 0.01$$

Magnesium ferrite

Mixture of MgFe_2O_4 and iron powder



$$\frac{f_{\text{Fe}_A^{3+}}}{f_{\text{Fe}}} = \left(\frac{1}{\lambda}\right) \left(\frac{m_{\text{Fe}}}{m_T}\right) \left(\frac{\mu_T}{\mu_{\text{Fe}}}\right) \frac{\left(\frac{A_M}{A_{\text{Fe}}}-1\right)}{\left(\frac{A_{\text{Fe}_B^{3+}}}{A_{\text{Fe}_A^{3+}}} + 1\right)}$$

$$\frac{f_{\text{Fe}_B^{3+}}}{f_{\text{Fe}}} = \left(\frac{1}{2-\lambda}\right) \left(\frac{m_{\text{Fe}}}{m_T}\right) \left(\frac{\mu_T}{\mu_{\text{Fe}}}\right) \frac{\left(\frac{A_M}{A_{\text{Fe}}}-1\right)}{\left(\frac{A_{\text{Fe}_A^{3+}}}{A_{\text{Fe}_B^{3+}}} + 1\right)}$$

The RT recoilless f-factor ratio of $f_{\text{Fe}_A^{3+}}/f_{\text{Fe}}$ and $f_{\text{Fe}_B^{3+}}/f_{\text{Fe}}$ were 0.91 and 1.38, respectively.
Quotient of these two f-factors $f_{\text{Fe}_B^{3+}}/f_{\text{Fe}_A^{3+}}$ is equal to 1.51.

3. $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$ ($x = 0$)

Cation Vacancies in NiFe_2O_4 During Heat Treatments

- (a) Mixture NiO and $\alpha\text{-Fe}_2\text{O}_3$
- (b) 1000 °C
- (c) 1100 °C
- (d) 1200 °C.

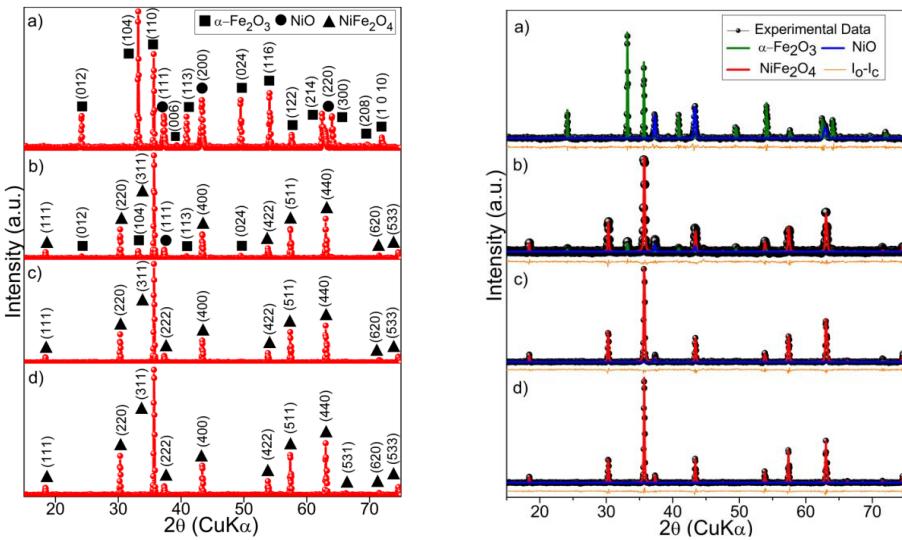


Table 1. Variation with temperature of the relative abundances and of the lattice parameter of NiFe_2O_4 . The conventional statistical parameters χ^2 , R_{wp} and R_{exp} were obtained from the Rietveld analysis of the XRD patterns. Estimated errors are of about 1 wt. % for the phase abundances and of 0.001 Å for the lattice parameters.

Sample	NiO (wt.%)	$\alpha\text{-Fe}_2\text{O}_3$ (wt.%)	NiFe_2O_4 (wt.%)	a (Å) (NiFe_2O_4)	R_{wp} (%)	R_{exp} (%)	χ^2
Initial mixture	32	68	---	---	9.23	7.65	1.46
1000 °C	6	13	81	8.333	8.46	7.11	1.42
1100 °C	< 1*	< 2*	97	8.336	7.27	6.35	1.31
1200 °C	---	---	100	8.340	7.65	6.58	1.35

*Values below or near to the XRD detection limit.

$$a_{th} = a_0 + m \lambda \quad (1)$$

in which λ is the inversion parameter, and:

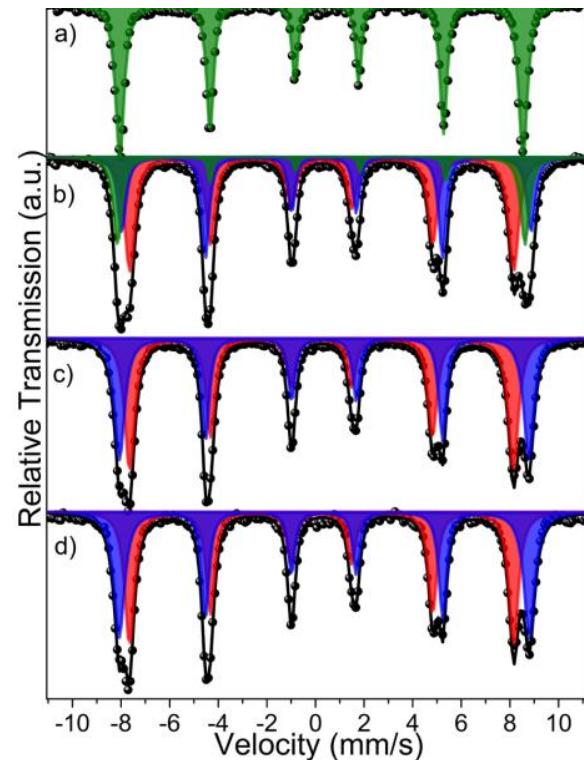
$$a_0 = \frac{8}{3\sqrt{3}} [r_{\text{Ni}_A^{2+}} + (\sqrt{3})r_{\text{Fe}_B^{3+}} + (1 + \sqrt{3})R_0] = 8.371 \text{ Å} \quad (2)$$

$$m = \frac{8}{3\sqrt{3}} \left[-r_{\text{Ni}_A^{2+}} + \left(\frac{\sqrt{3}}{2}\right)r_{\text{Ni}_B^{3+}} + r_{\text{Fe}_A^{3+}} - \left(\frac{\sqrt{3}}{2}\right)r_{\text{Fe}_B^{3+}} \right] = -0.032 \text{ Å} \quad (3)$$

$$8.339 \text{ Å } (\lambda = 1) \leq a_{th} \leq 8.371 \text{ Å } (\lambda = 0)$$

Table 2. Hyperfine parameters for the (A) and [B] sites of NiFe₂O₄. δ_A and δ_B are the isomer shifts, $2\epsilon_A$ and $2\epsilon_B$ are the quadrupole shifts, B_A and B_B are the hyperfine magnetic fields, and A_A and A_B are the relative spectral areas for irons at (A) and [B] sites, respectively.

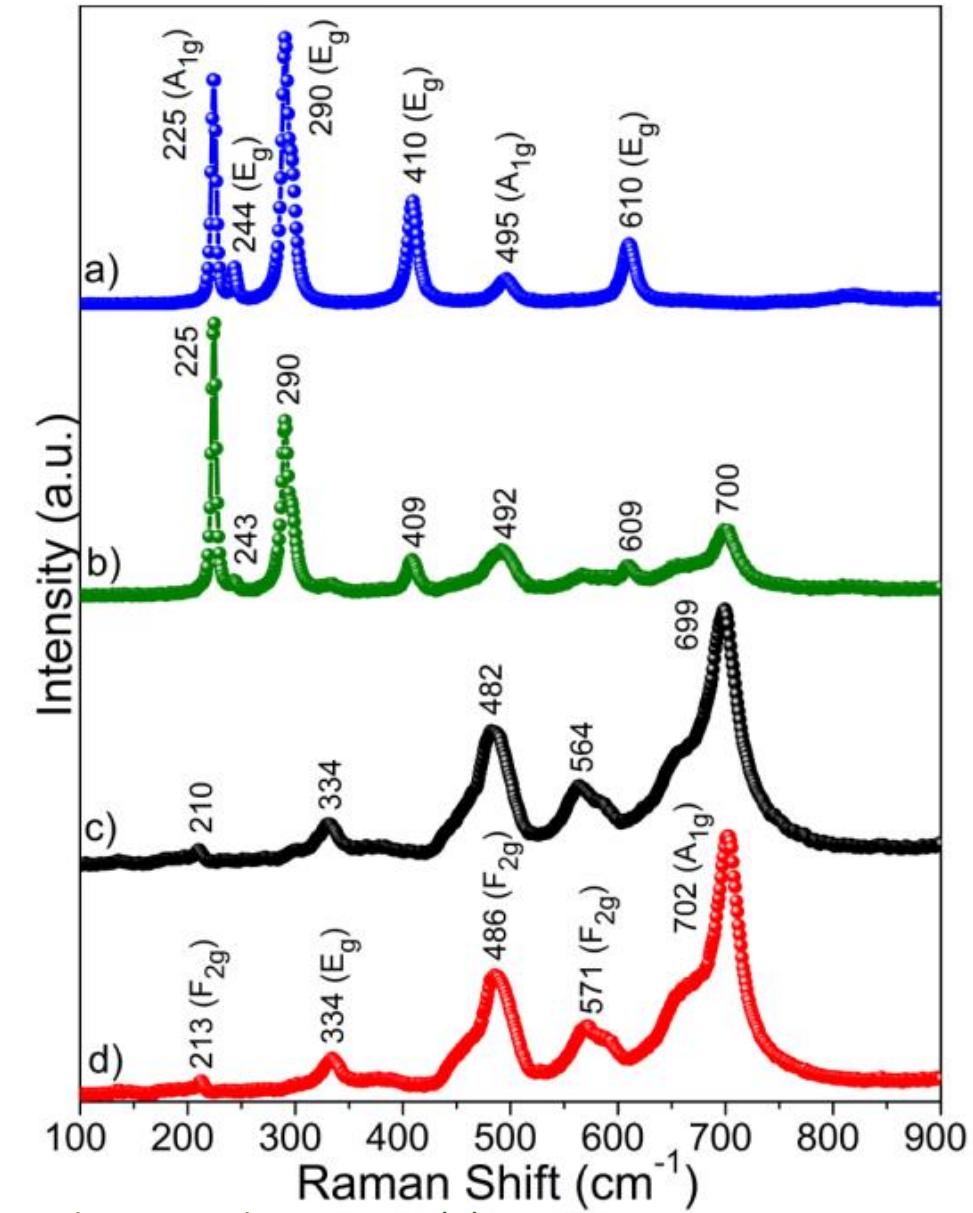
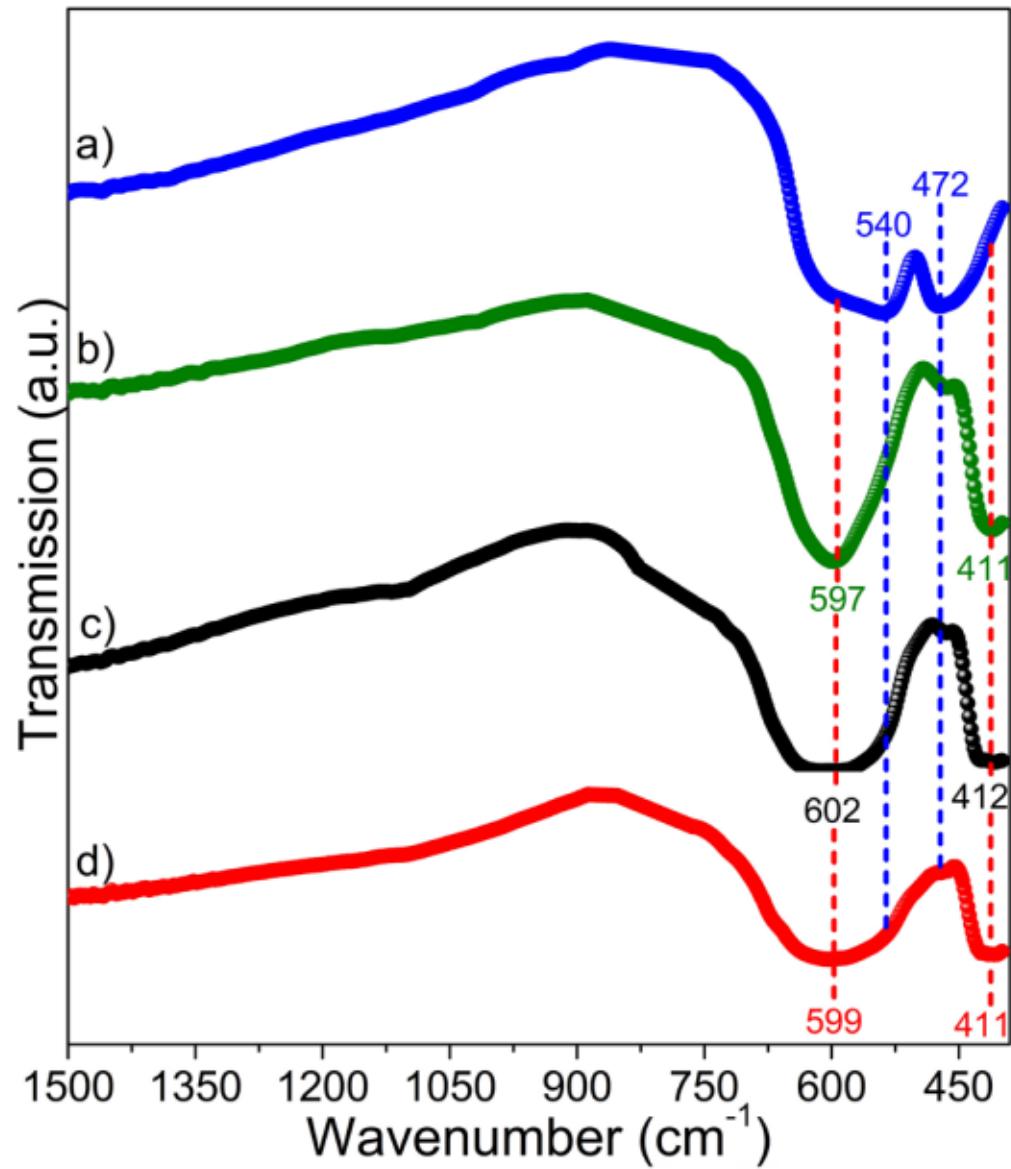
Sample	δ_A (mm/s)	$2\epsilon_A$ (mm/s)	B_A (T)	A_A (%)	δ_B (mm/s)	$2\epsilon_B$ (mm/s)	B_B (T)	A_B (%)	A_A/A_B
1000 °C	0.25	0	49	45	0.36	0	52.3	27	1.67
1100 °C	0.25	0	49	52	0.36	0	52.3	48	1.08
1200 °C	0.25	0	49	50	0.36	0	52.3	50	1



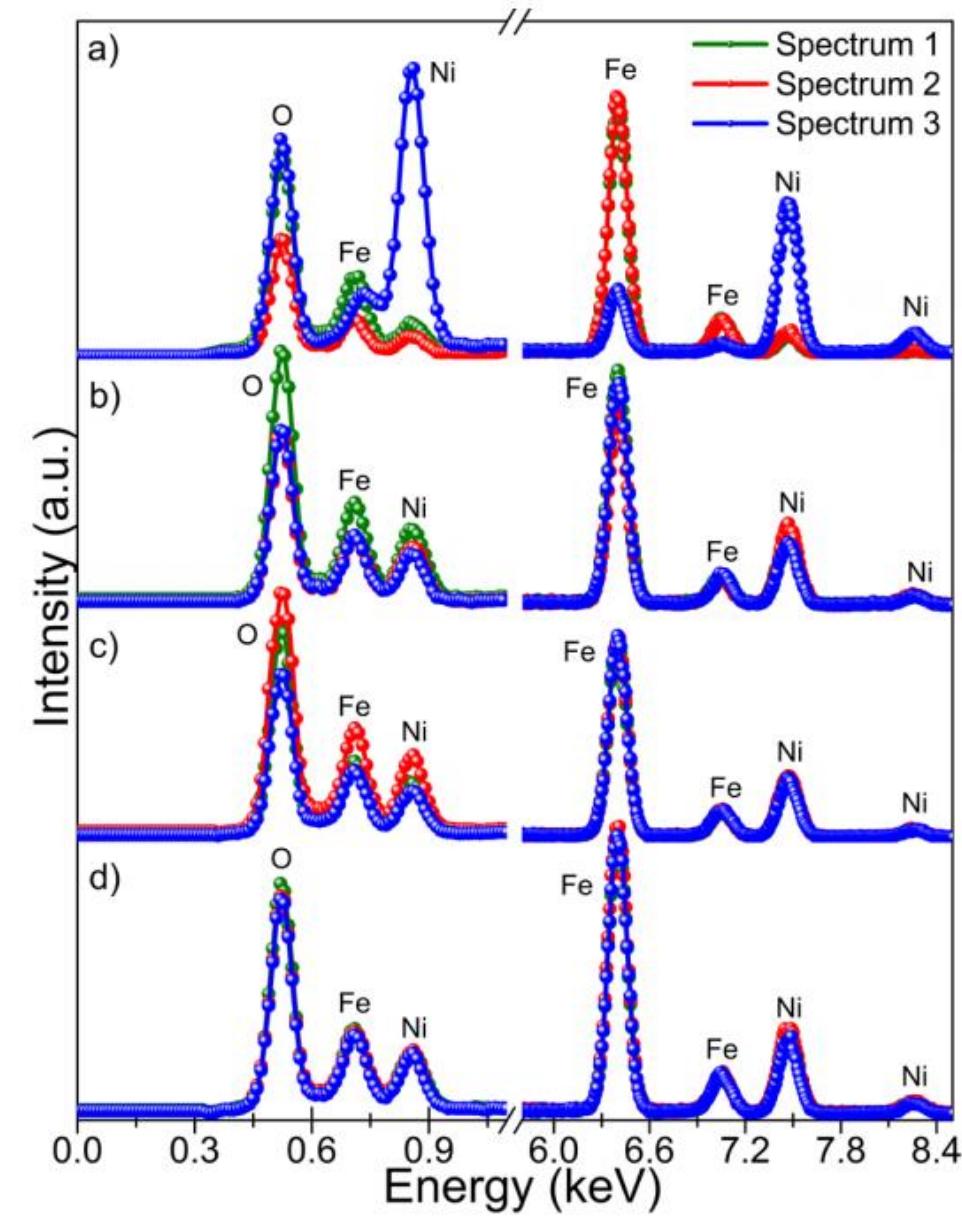
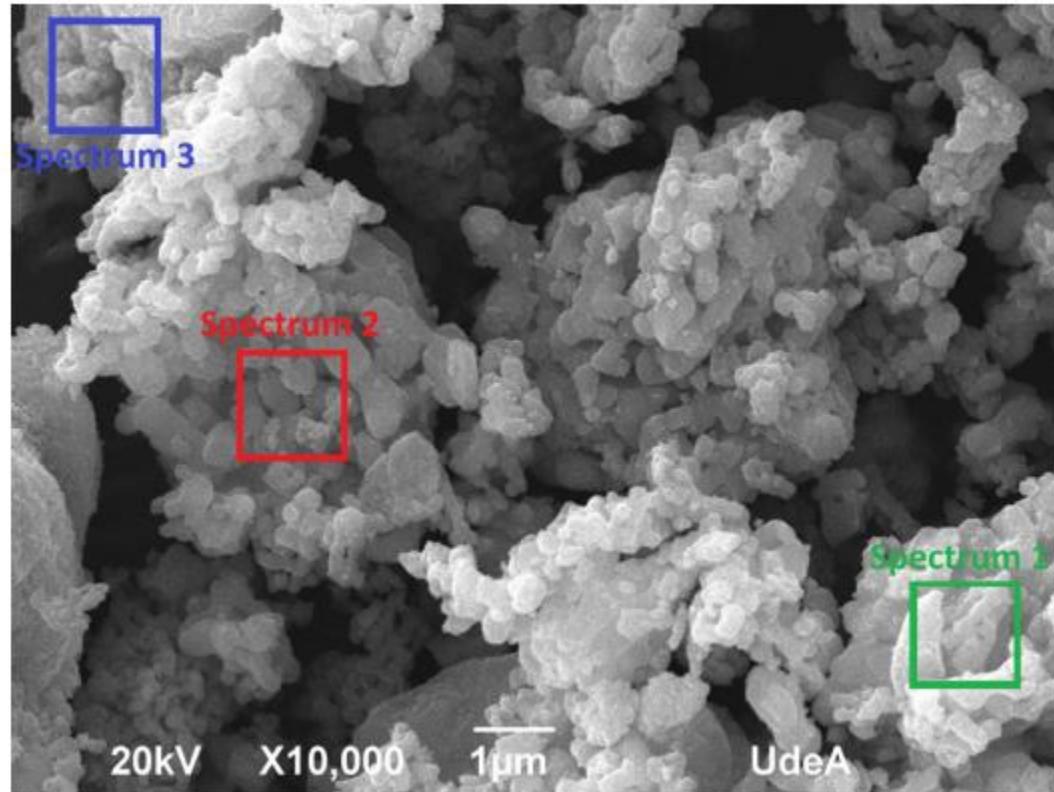
$$\frac{A_A}{A_B} = \left(\frac{f_A}{f_B} \right) \left(\frac{\lambda}{2 - \lambda} \right)$$

where $\frac{f_A}{f_B}$ is the recoilless *f*-factors ratio for Fe³⁺ cations at (A) and [B] sites. Using equation (4) and considering $\frac{f_B}{f_A}$ at room temperature (RT) [24]; we found $\frac{A_A}{A_B} = 0$ for $\lambda = 0$, and $\frac{A_A}{A_B} = 0.92$ for $\lambda = 1$. Notice that the experimental values of $\frac{A_A}{A_B}$ reported in Table 2 are outside the range of expected

IR and Raman spectra of (a) the initial mixture of reactants, (b) 1000 °C, (c) 1100 °C and (d) 1200 °C.



SEM micrograph and EDS spectra



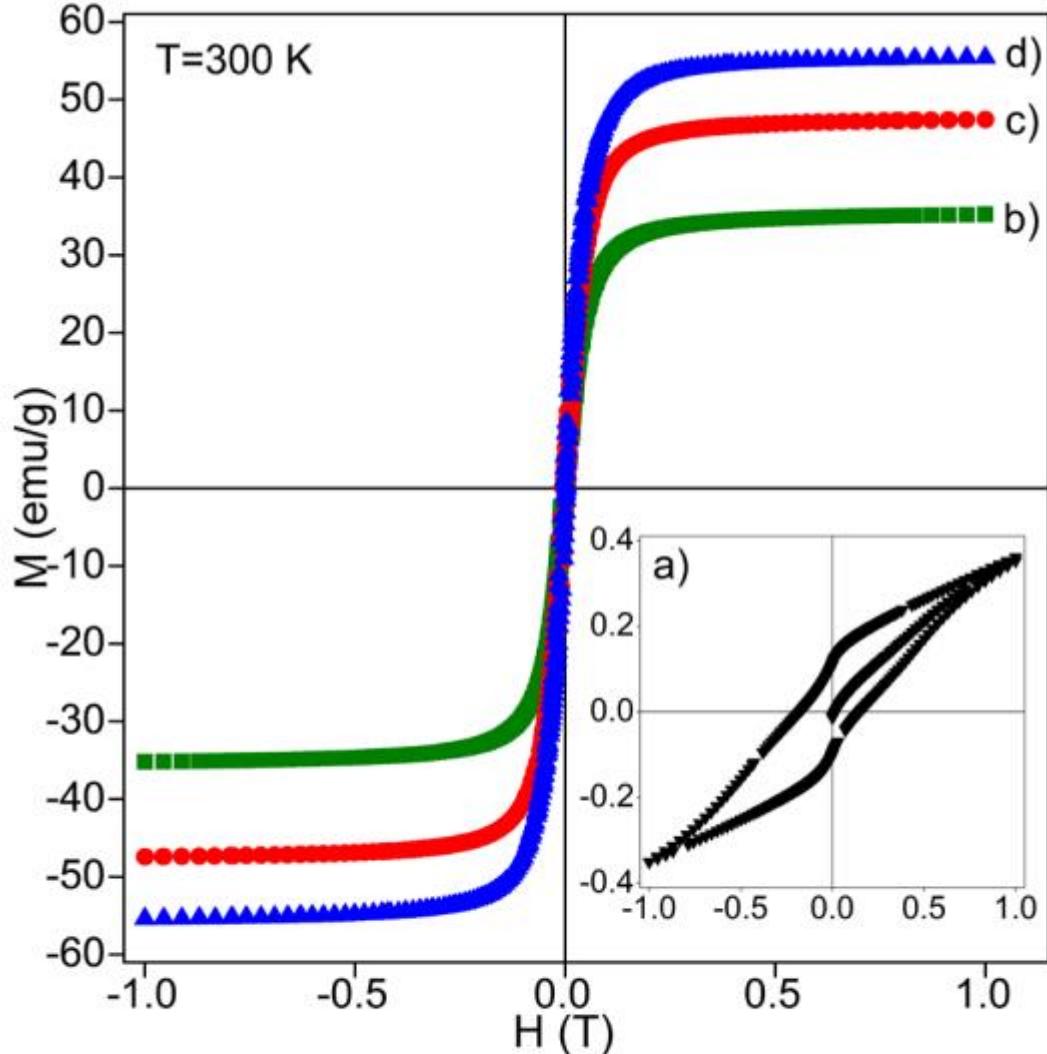


Figure 9. Hysteresis loops of (a) the initial mixture of reactants and of the samples submitted to heat treatments at (b) 1000 °C, (c) 1100 °C and (d) 1200 °C.

Table 3. Saturation magnetization (M_s), remanent magnetization (M_R) and coercive magnetic field (H_c) values obtained in the analysis of the hysteresis loops.

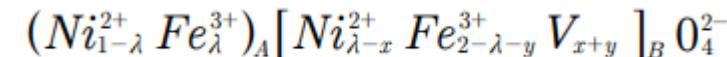
Sample	M_s (emu/g)	M_R (emu/g)	H_c (10^{-3} T)
Initial mixture	0.4	0.1	160
1000 °C	35.2	4.0	5.0
1100 °C	47.4	4.0	4.6
1200 °C	55.4	4.4	3.2



$$M_A = (1 - \lambda)M_{Ni^{2+}} + \lambda M_{Fe^{3+}}$$

$$M_B = \lambda M_{Ni^{2+}} + (2 - \lambda)M_{Fe^{3+}}$$

$$M_{the} = 2(4 - 3\lambda)\mu_B$$



$$M_{the} = [2(4 - 3\lambda) - (2x + 5y)]\mu_B$$

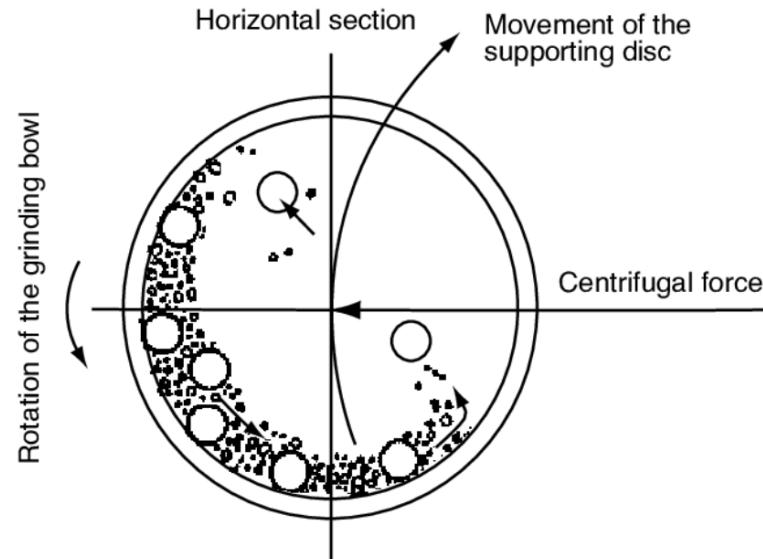
3. $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$ ($x \neq 0$)

Synthesis by solid state reaction

Step 1: Stoichiometric calculations.

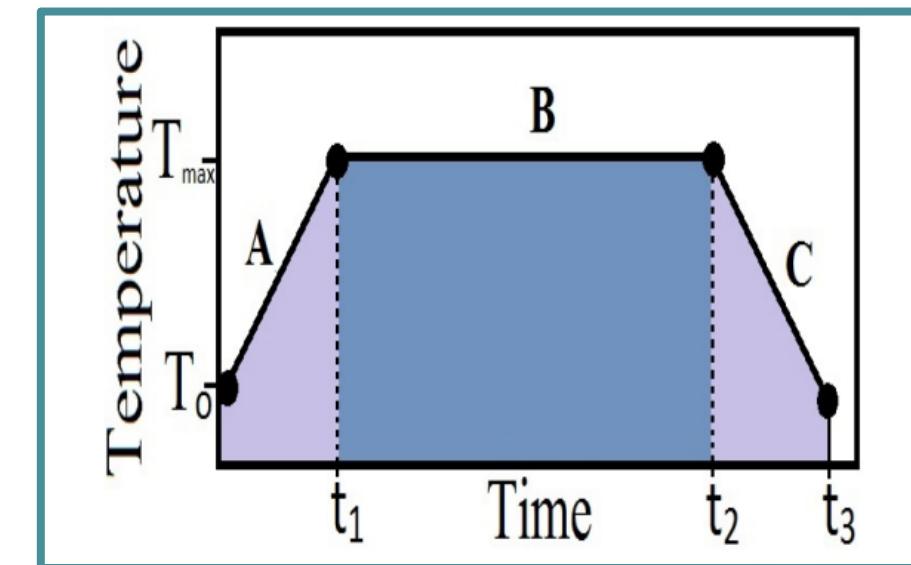
Step 2: Mechanical Milling.

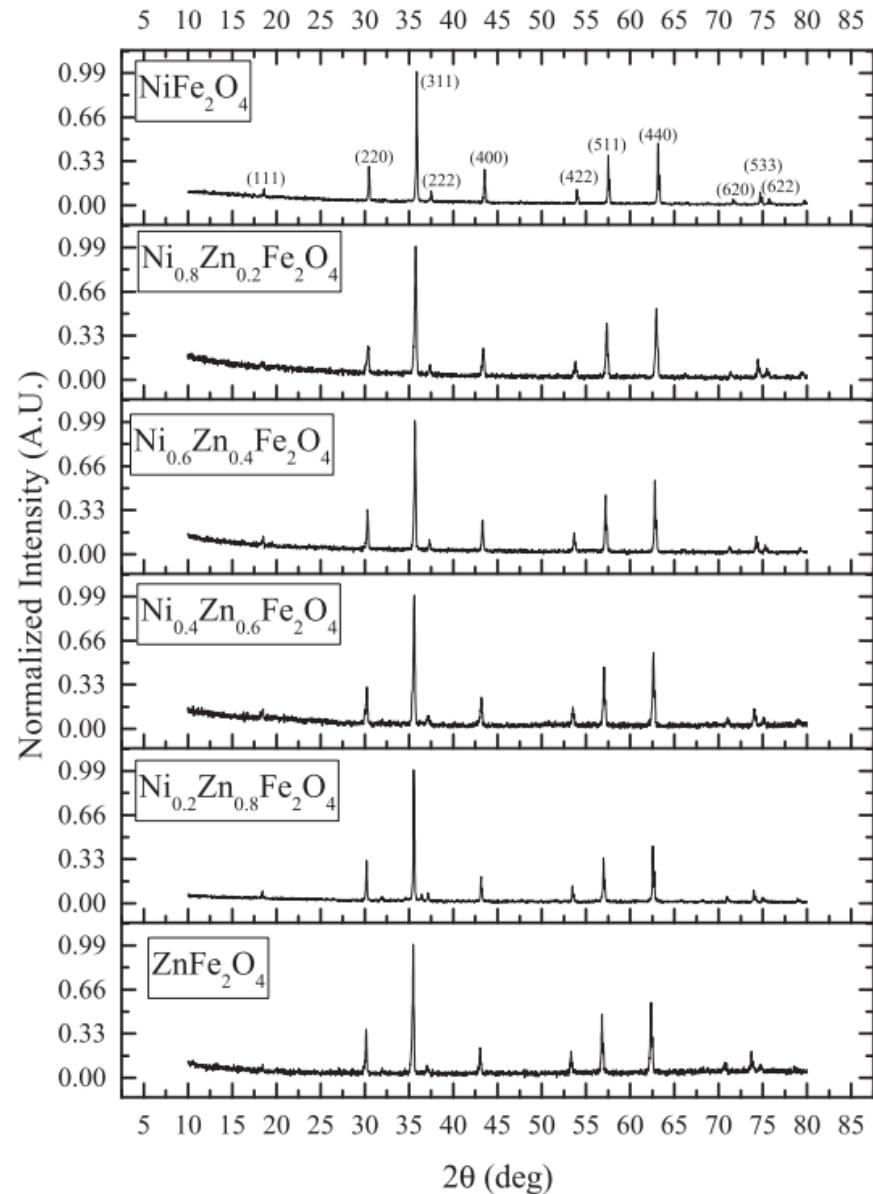
- Obtain a homogeneous mixture.
- Reduce the particle size.
- Increase the contact area between the reactants



Step 3: Solid-State Reaction.

- Heating Rate: 2 °C/min.
- Maximum Temperature: 1250 °C.
- Thermal Treatment: 15 h.
- Cooling Rate: 10 °C/min.

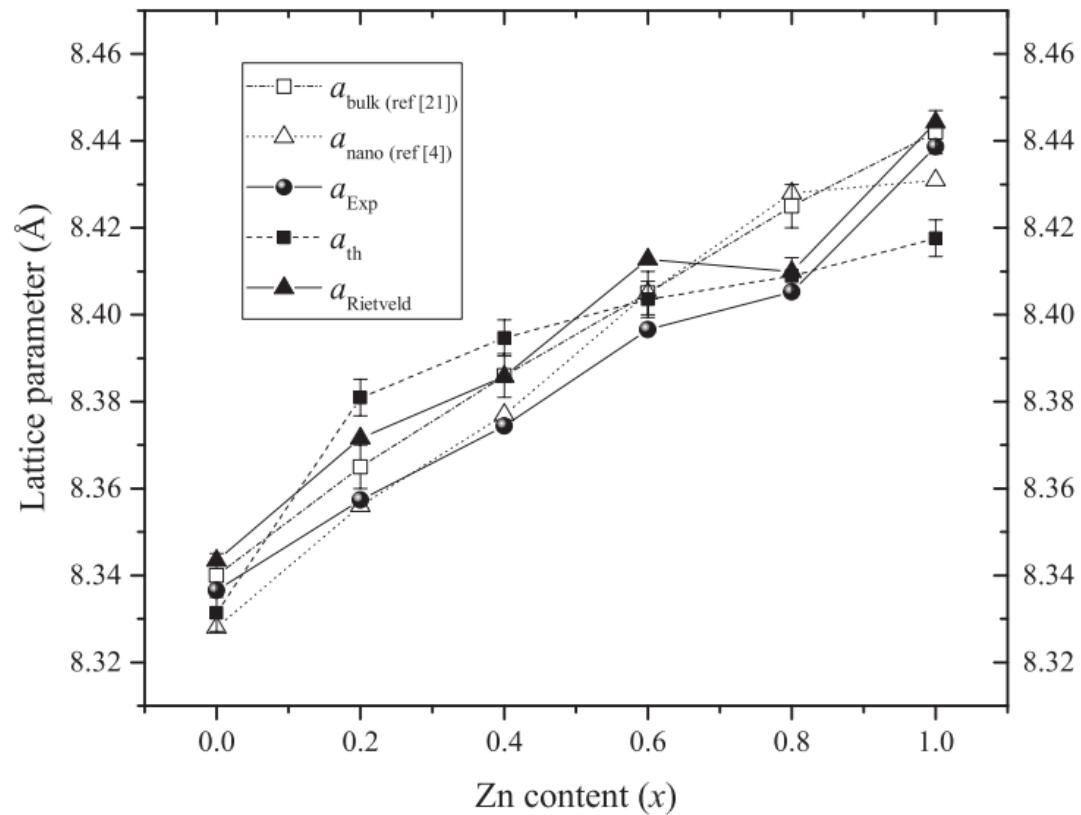




$$r_{\text{Tetra}} = |C_{\text{Ni}} r_{\text{Ni}^{2+}} + C_{\text{Zn}} r_{\text{Zn}^{2+}} + C_{\text{Fe}} r_{\text{Fe}^{3+}}|$$

$$r_{\text{Octa}} = 1/2 |C_{\text{Ni}} r_{\text{Ni}^{2+}} + C_{\text{Zn}} r_{\text{Zn}^{2+}} + C_{\text{Fe}} r_{\text{Fe}^{3+}}|$$

$$a_{\text{th}} = \frac{8}{3\sqrt{3}} [(r_{\text{Tetra}} + r_o) + \sqrt{3}(r_{\text{Octa}} + r_o)]$$



S.A. Mazen et al., Phys. Status Solidi A. 134 (1992) 263

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Estimated cation distribution and X-ray intensity ratios for the $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$ ferrites.

x	Cation Distribution*	$I_{(220)} / I_{(440)}$		$I_{(400)} / I_{(220)}$		$\frac{\text{Fe}^{3+} \text{ Tetra}}{\text{Fe}^{3+} \text{ Octa}}$
		Obs.	Calc.	Obs.	Calc.	
0.0	($\text{Fe}_{1.000}$) [$\text{Ni}_{1.000}\text{Fe}_{1.000}$]	0.506	0.802	1.049	3.454	1.000
0.2	($\text{Ni}_{0.512}\text{Zn}_{0.200}\text{Fe}_{0.288}$) [$\text{Ni}_{0.288}\text{Zn}_{0.000}\text{Fe}_{1.712}$]	0.387	0.513	0.991	2.463	0.168
0.4	($\text{Ni}_{0.456}\text{Zn}_{0.400}\text{Fe}_{0.144}$) [$\text{Ni}_{0.144}\text{Zn}_{0.00}\text{Fe}_{1.856}$]	0.458	0.633	0.878	2.184	0.078
0.6	($\text{Ni}_{0.380}\text{Zn}_{0.497}\text{Fe}_{0.123}$) [$\text{Ni}_{0.020}\text{Zn}_{0.103}\text{Fe}_{1.877}$]	0.410	0.537	0.864	2.164	0.066
0.8	($\text{Ni}_{0.153}\text{Zn}_{0.766}\text{Fe}_{0.081}$) [$\text{Ni}_{0.047}\text{Zn}_{0.034}\text{Fe}_{1.919}$]	0.556	0.814	0.886	1.985	0.042
1.0	($\text{Zn}_{1.000}$) [$\text{Fe}_{2.000}$]	0.416	0.519	0.693	1.834	0.000

* Round () and square [] brackets denote, respectively, tetrahedral and octahedral coordination sites.

$$I_{hkl} = |F_{hkl}|^2 p L_p$$

$$L_p = \frac{1 + \cos^2 2\theta}{\sin^2 \theta \cos \theta}$$

$$f_a = (\text{Zn}_x)f_{\text{Zn}} + (\text{Fe}_{1-x})f_{\text{Fe}}$$

$$f_b = (\text{Ni}_{1-x})f_{\text{Ni}} + (\text{Fe}_{1+x})f_{\text{Fe}}$$

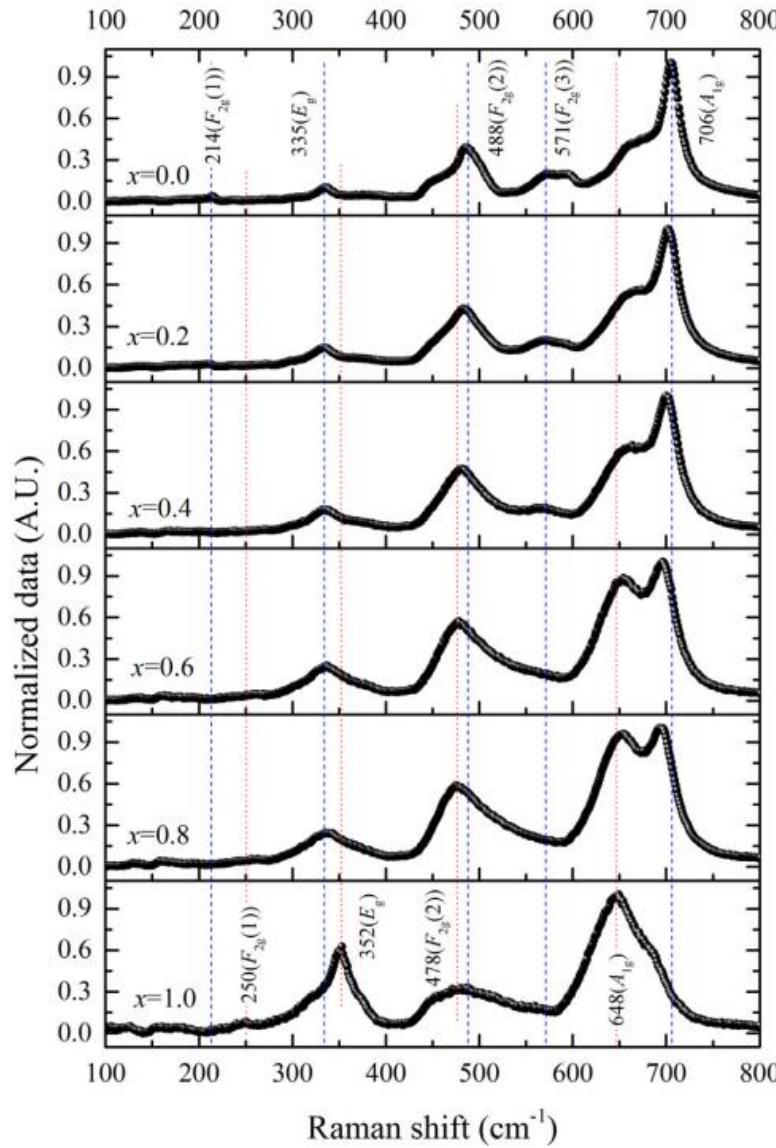
$$F_{220} = -8f_a$$

$$F_{400} = 8(f_a - 2f_b - 4f_o)$$

$$F_{440} = 8(f_a + 2f_b + 4f_o)$$

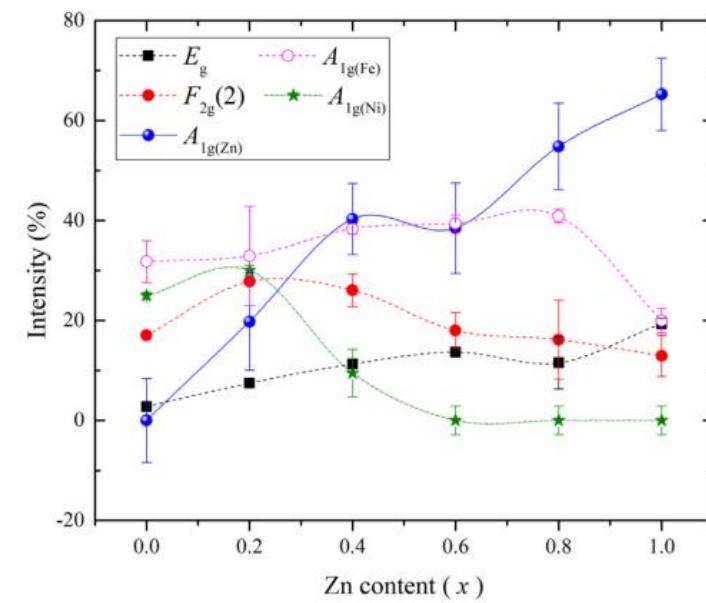
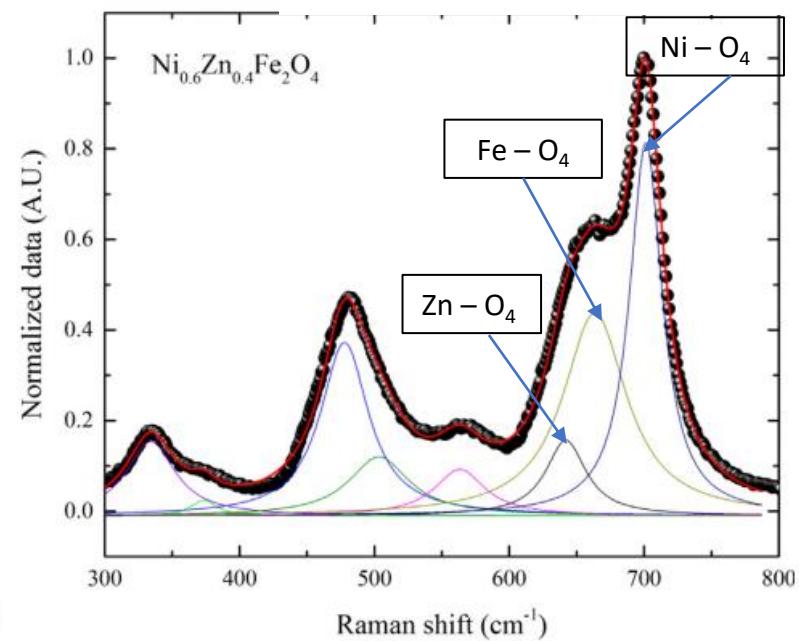
$$F_{422} = 8f_a$$



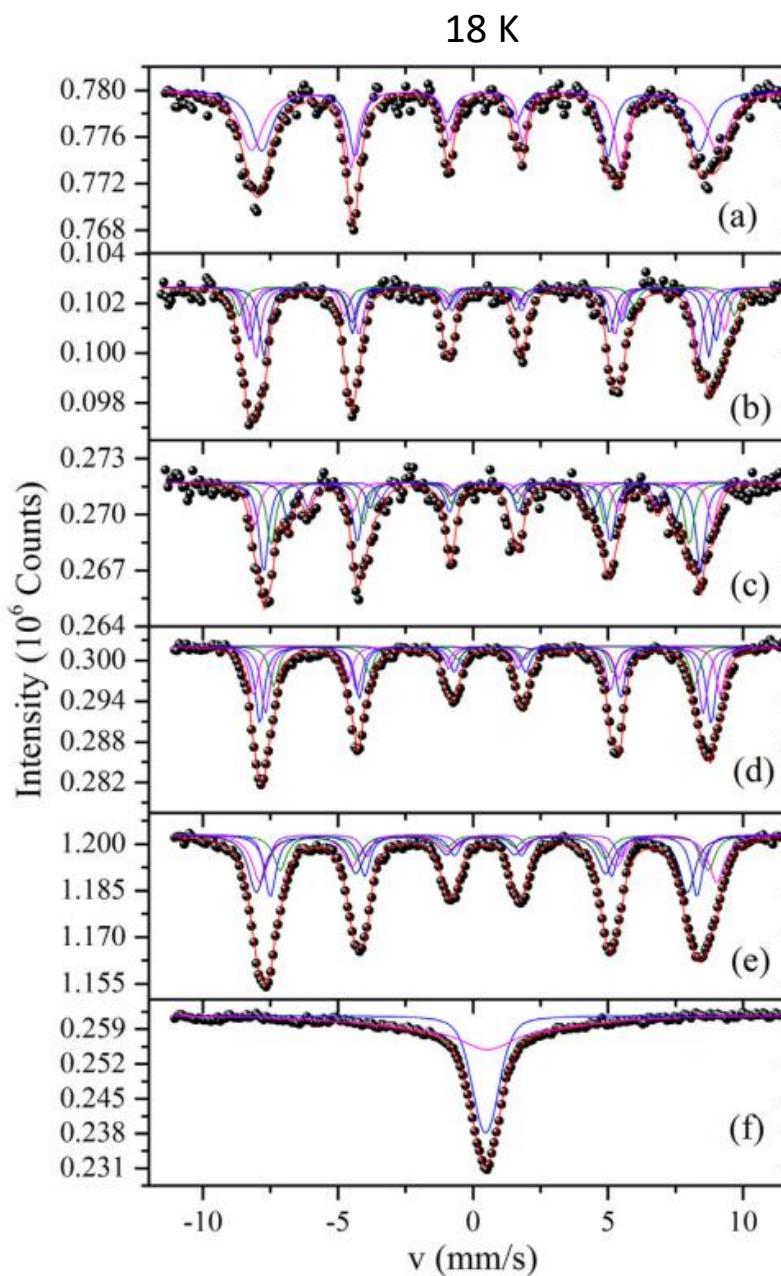
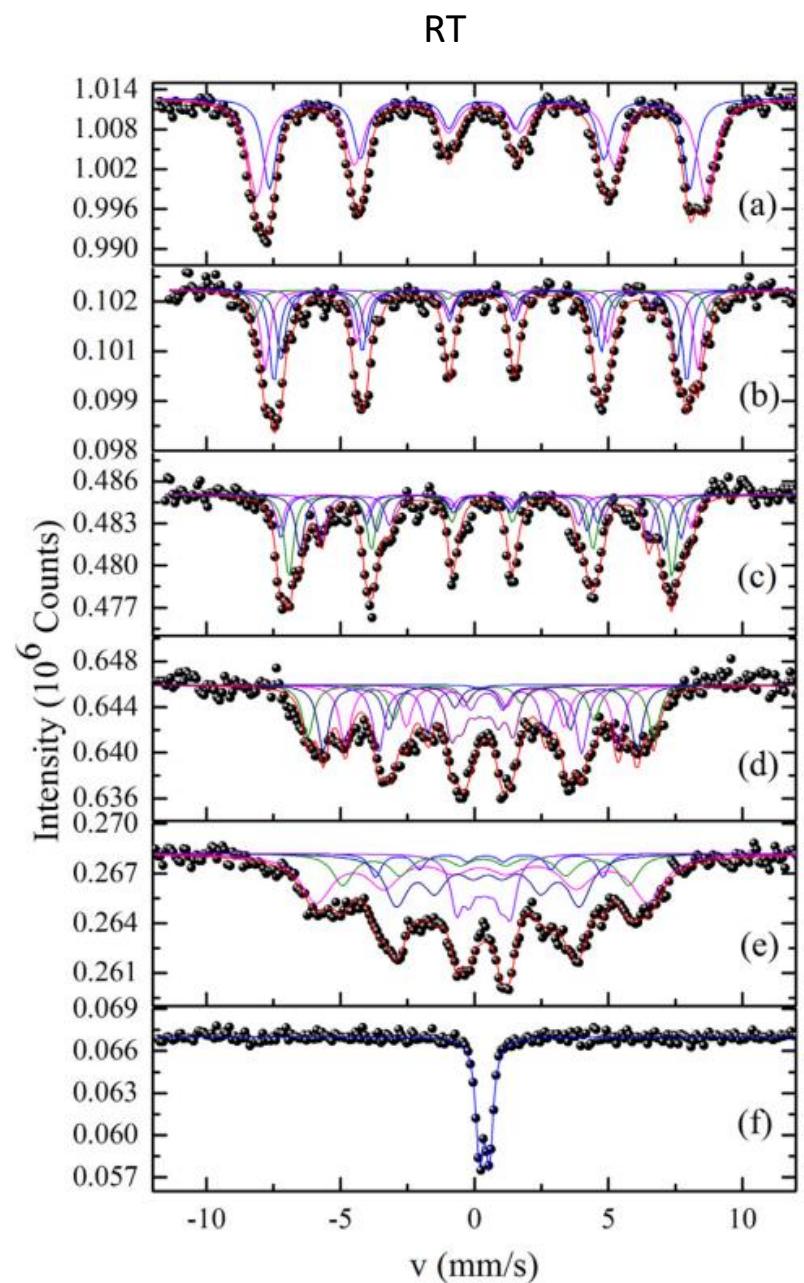


Location of the main Raman active modes for the $\text{Ni}_{1-x}\text{Zn}_x\text{Fe}_2\text{O}_4$ ($x = 0.0, 0.2, 0.4, 0.6, 0.8$ and 1.0) ferrites.

Raman active mode	Raman shift (cm^{-1})					
	$x = 0.0$	$x = 0.2$	$x = 0.4$	$x = 0.6$	$x = 0.8$	$x = 1.0$
$F_{2g}(1)$	214.15	214.00	214.00	—	—	250.1
E_g	334.86	332.64	334.17	333.86	338.92	351.71
$F_{2g}(2)$	488.17	484.95	477.84	470.97	476.75	478.11
$F_{2g}(3)$	571.06	566.92	563.36	—	—	—
A_{1g}	705.94	703.14	701.35	660.18 and 696.83	656.20 and 695.62	648.06



$$\text{Zn}_x = I_{\text{Zn}} / (I_{\text{Zn}} + I_{\text{Ni}} + I_{\text{Fe}})$$



Based on Leung, Evans and Morrish, Phys. Rev. B. 8 (1973) 29

$$\langle B_{octa}(x, T) \rangle_{th} = B_{octa}(0, T) - \sum_{n=0}^6 P(n, x) \Delta B_{octa}(n, T)$$

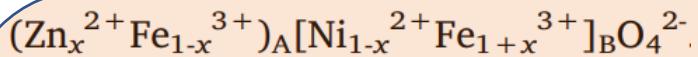
$$P(n, x) = \frac{6!}{n!(6-n)!} (x)^n (1-x)^{6-n}$$

$$\langle B_{octa}(x, T) \rangle_{th} = B_{octa}(0, T) - \sum_{n=0}^6 n P(n, x) \Delta B_{octa}(1, T)$$

$$\Delta B_{octa}(1, T) = \frac{B_{octa}(0, T) - \langle B_{octa}(x, T) \rangle_{exp}}{\sum_{n=0}^6 n P(n, x)}$$

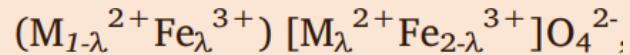
$$\Delta B_{octa}(1, 18K) = 0.9 \pm 0.5 \text{ T}$$

$Fe_A^{3+} - O^{2+} - Fe_B^{3+}$ superexchange interaction.



$$\left(\frac{A_{[B]}}{A_{(A)}} \right) = \left(\frac{1+x}{1-x} \right) \left(\frac{f_{[B]}}{f_{(A)}} \right)$$

$$x = \frac{\left(\frac{A_{[B]}}{A_{(A)}} \right) - \left(\frac{f_{[B]}}{f_{(A)}} \right)}{\left(\frac{A_{[B]}}{A_{(A)}} \right) + \left(\frac{f_{[B]}}{f_{(A)}} \right)}$$



V. Šepelák et al., J. Alloy. Compd. 434–435 (2007) 776

$$\lambda = \frac{2 \left(\frac{f_{[B]}}{f_{(A)}} \right)}{\frac{A_{[B]}}{A_{(A)}} + \frac{f_{[B]}}{f_{(A)}}}$$

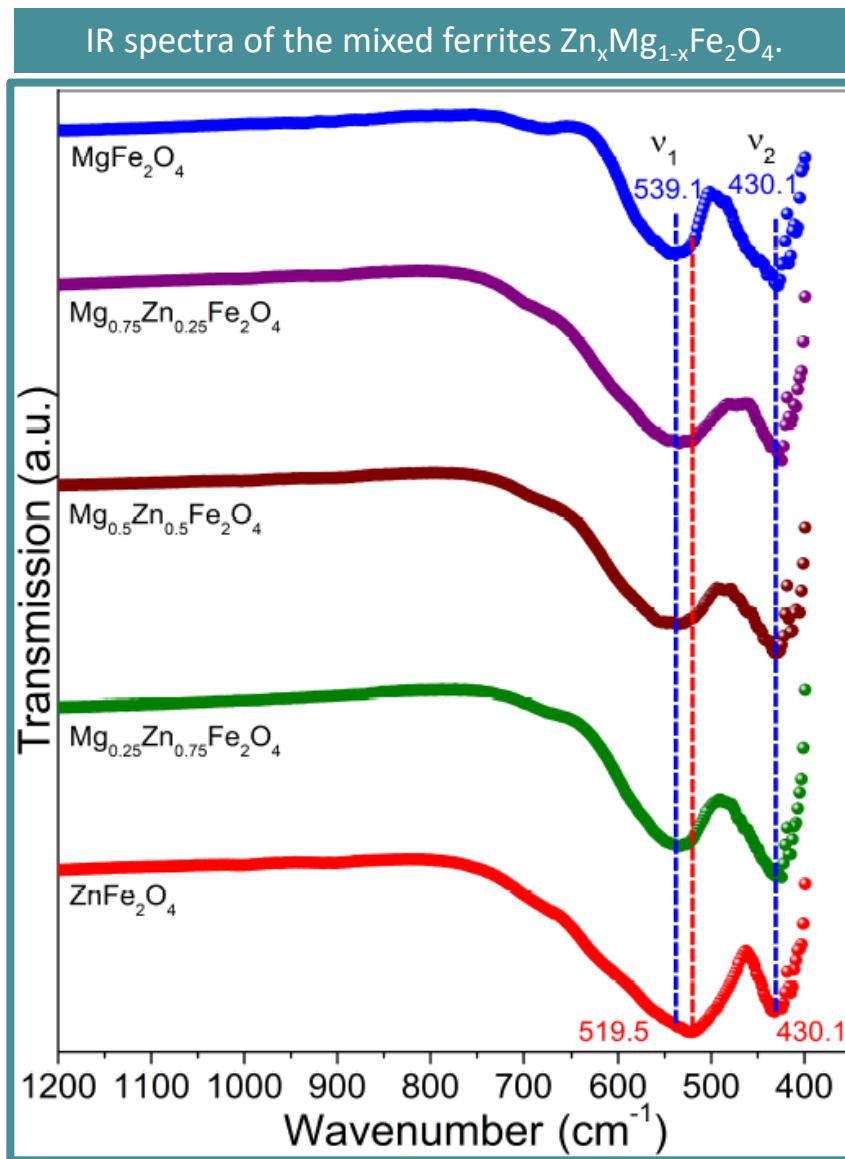
Comparison of the Zn content (x values) at the tetrahedral sites as obtained from the three characterization techniques.

Nominal sample	X-Ray Diffraction*	Raman spectroscopy	18 K Mössbauer spectroscopy
$NiFe_2O_4$ ($x = 0.0$)	0.00	0.00	0.05
$Ni_{0.8}Zn_{0.2}Fe_2O_4$ ($x = 0.2$)	0.20	0.24	0.46
$Ni_{0.6}Zn_{0.4}Fe_2O_4$ ($x = 0.4$)	0.40	0.46	0.52
$Ni_{0.4}Zn_{0.6}Fe_2O_4$ ($x = 0.6$)	0.50	0.49	0.66
$Ni_{0.2}Zn_{0.8}Fe_2O_4$ ($x = 0.8$)	0.77	0.57	0.70
$ZnFe_2O_4$ ($x = 1.0$)	1.00	0.77	1.00

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4. $Mg_{1-x}Zn_xFe_2O_4$



There are two main absorption bands that are unrelated to the reactants ZnO, MgO, and α -Fe₂O₃.

Sample	ν_1 (cm ⁻¹)	ν_2 (cm ⁻¹)
$MgFe_2O_4$	539.1	430.1
$Zn_{0.25}Mg_{0.75}Fe_2O_4$	535.1	430.1
$Zn_{0.5}Mg_{0.5}Fe_2O_4$	534.1	430.1
$Zn_{0.75}Mg_{0.25}Fe_2O_4$	532.3	430.1
$ZnFe_2O_4$	519.5	430.1

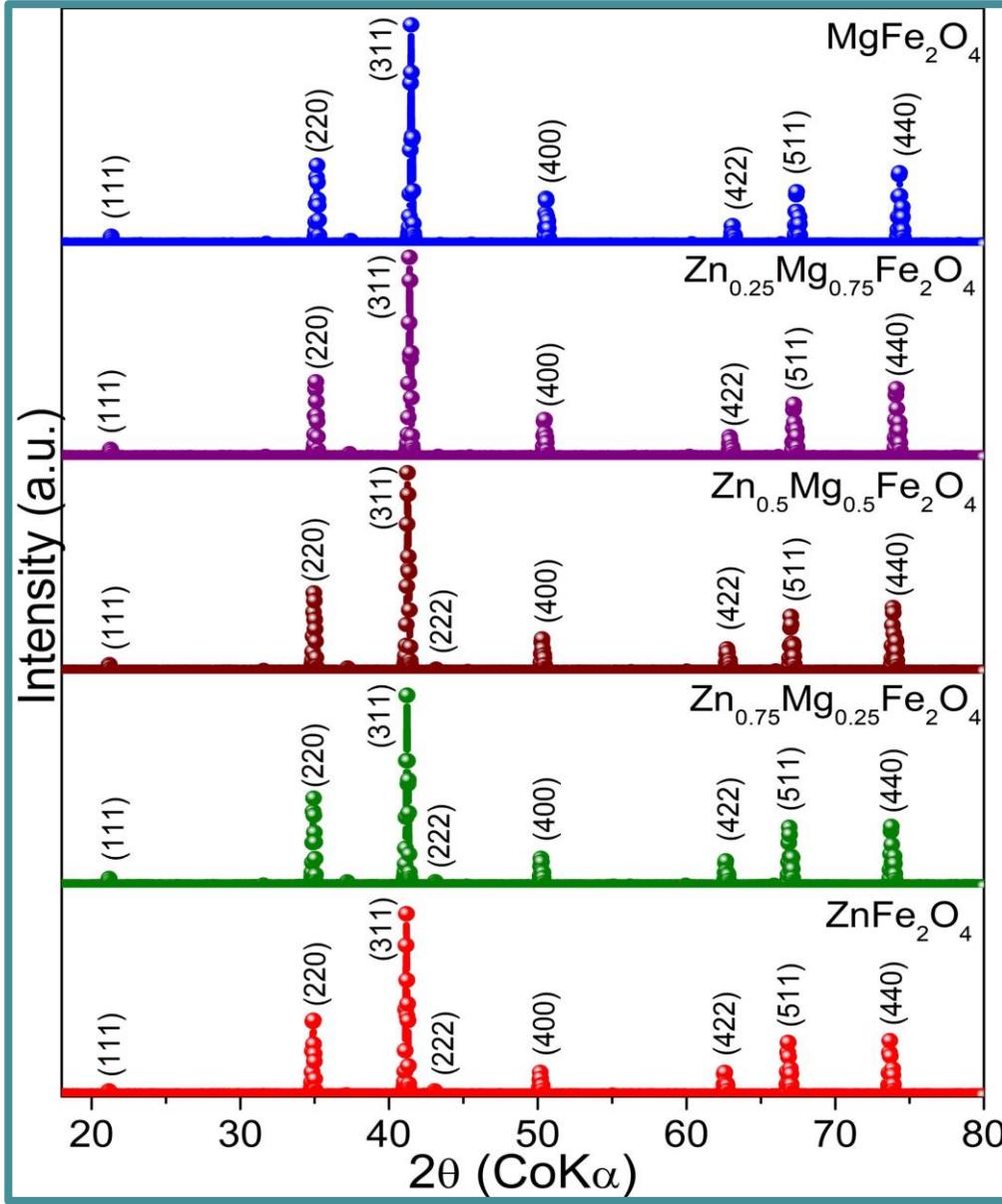
Infrared absorption bands of mixed ferrites $Zn_xMg_{1-x}Fe_2O_4$.

- ν_1 corresponds to stretching vibrations of the Fe³⁺-O²⁻ bonds (A sites).
- ν_2 corresponds to metal-oxygen vibrations (B sites).

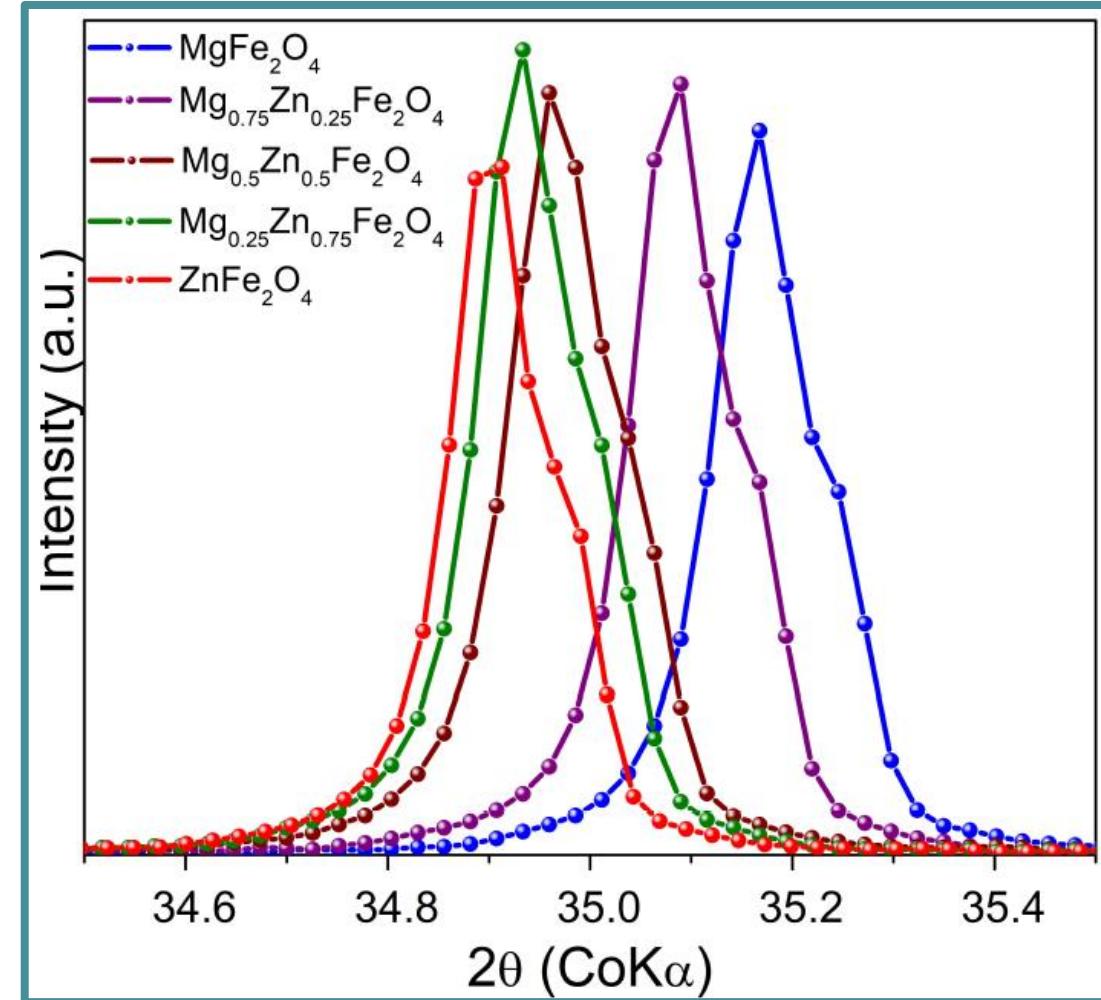
Fe-O bond length at tetrahedral sites → 1.901-1.976 Å

Fe-O bond length at octahedral sites → 2.045-2.032 Å

XRD patterns of mixed ferrites $Zn_xMg_{1-x}Fe_2O_4$ for different concentrations of Zinc .

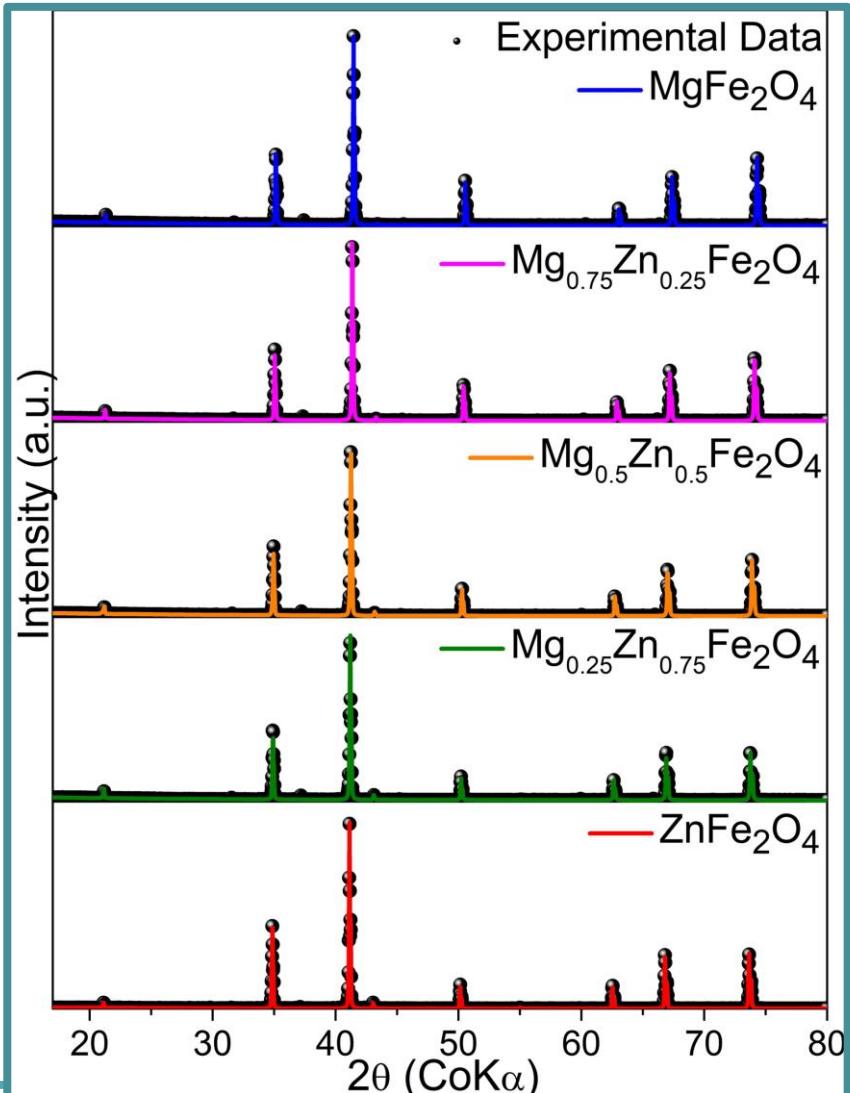


Displacement of the diffraction peaks (220) as a function of the Zn concentration.



Determining lattice parameters

Rietveld analysis of mixed ferrites
 $Zn_xMg_{1-x}Fe_2O_4$ for different concentrations of Zinc.



Rietveld analysis

The Rietveld method uses a least squares approach to refine a theoretical line profile until it matches the measured profile

Sample	Lattice parameter (Å)	Average crystallite size (Å)	Density (g.cm ⁻³)
$MgFe_2O_4$	8.379	762.68	4.51
$Zn_{0.25}Mg_{0.75}Fe_2O_4$	8.398	762.44	4.71
$Zn_{0.5}Mg_{0.5}Fe_2O_4$	8.418	762.11	4.91
$Zn_{0.75}Mg_{0.25}Fe_2O_4$	8.431	952.68	5.11
$ZnFe_2O_4$	8.442	761.89	5.32

Lattice parameter, average crystallite size and x-ray density of the mixed ferrites $Zn_xMg_{1-x}Fe_2O_4$, as a function of the Zn concentration.

Cation distribution

The cation distribution for the $Zn_xMg_{1-x}Fe_2O_4$ ferrites can be calculated

Theoretical lattice parameter

$$a_{th} = 8 \frac{r_A + R_o + \sqrt{3}(r_B + R_o)}{3\sqrt{3}}$$

r_A and r_B are the cations radii of element at the tetrahedral and octahedral sites, respectively and R_o is the oxygen ion radius.

$$r_A = (C_{Mg^{2+}}^A)(r_{Mg^{2+}}) + (C_{Zn^{2+}}^A)(r_{Zn^{2+}}) + (C_{Fe^{3+}}^A)(r_{Fe^{3+}})$$

$$r_B = \frac{(C_{Mg^{2+}}^B)(r_{Mg^{2+}}) + (C_{Zn^{2+}}^B)(r_{Zn^{2+}}) + (C_{Fe^{3+}}^B)(r_{Fe^{3+}})}{2}$$

C^A and C^B are the ionic concentration at the tetrahedral and octahedral sites, respectively.

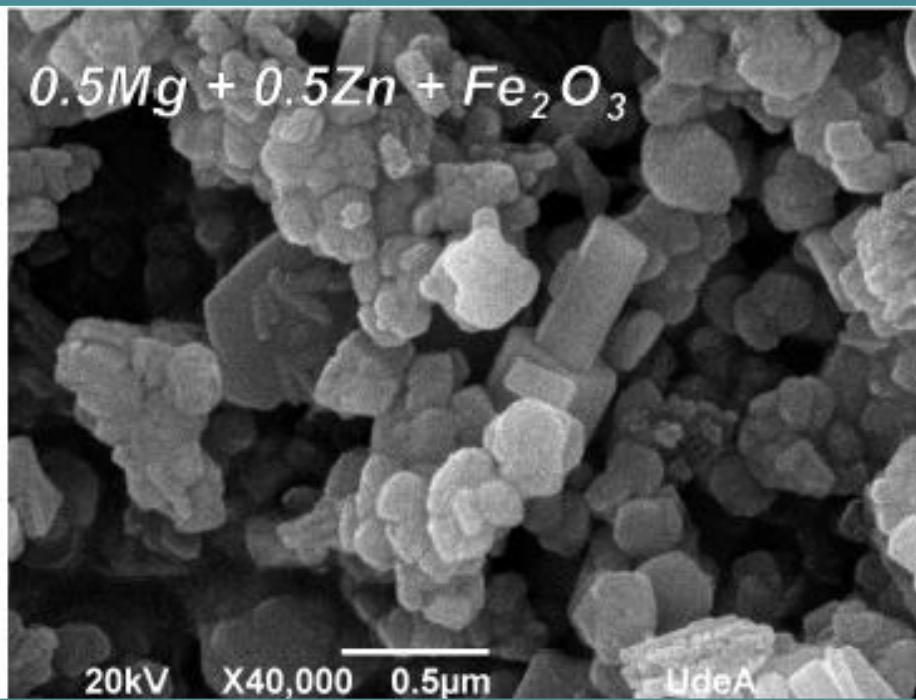
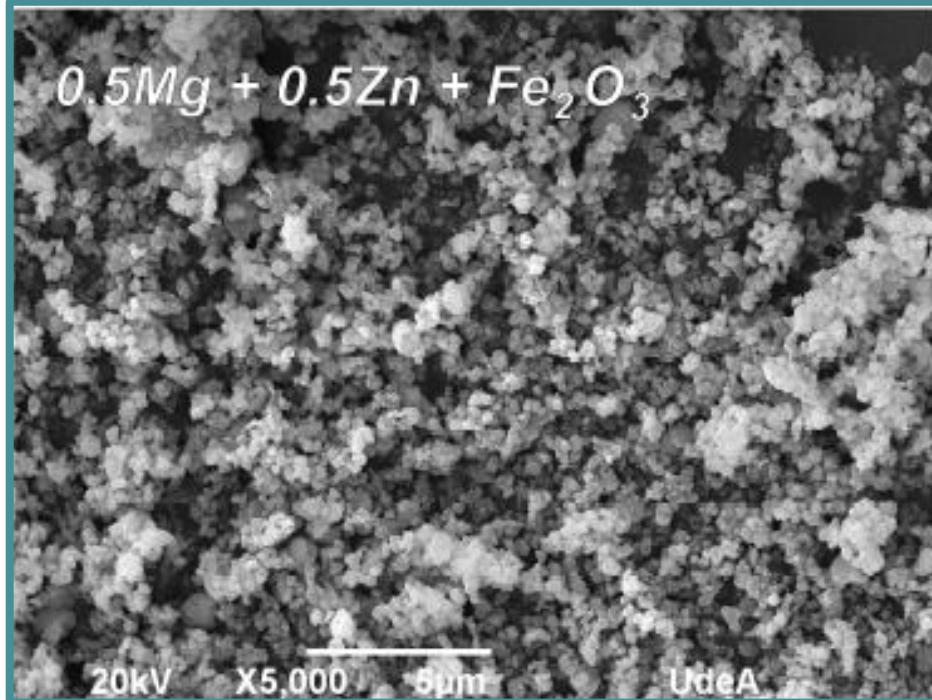
$r_{Mg^{2+}}$, $r_{Zn^{2+}}$ and $r_{Fe^{3+}}$ are the ionic radii of Mg^{2+} , Zn^{2+} and Fe^{3+} ions, respectively.

Cation distribution

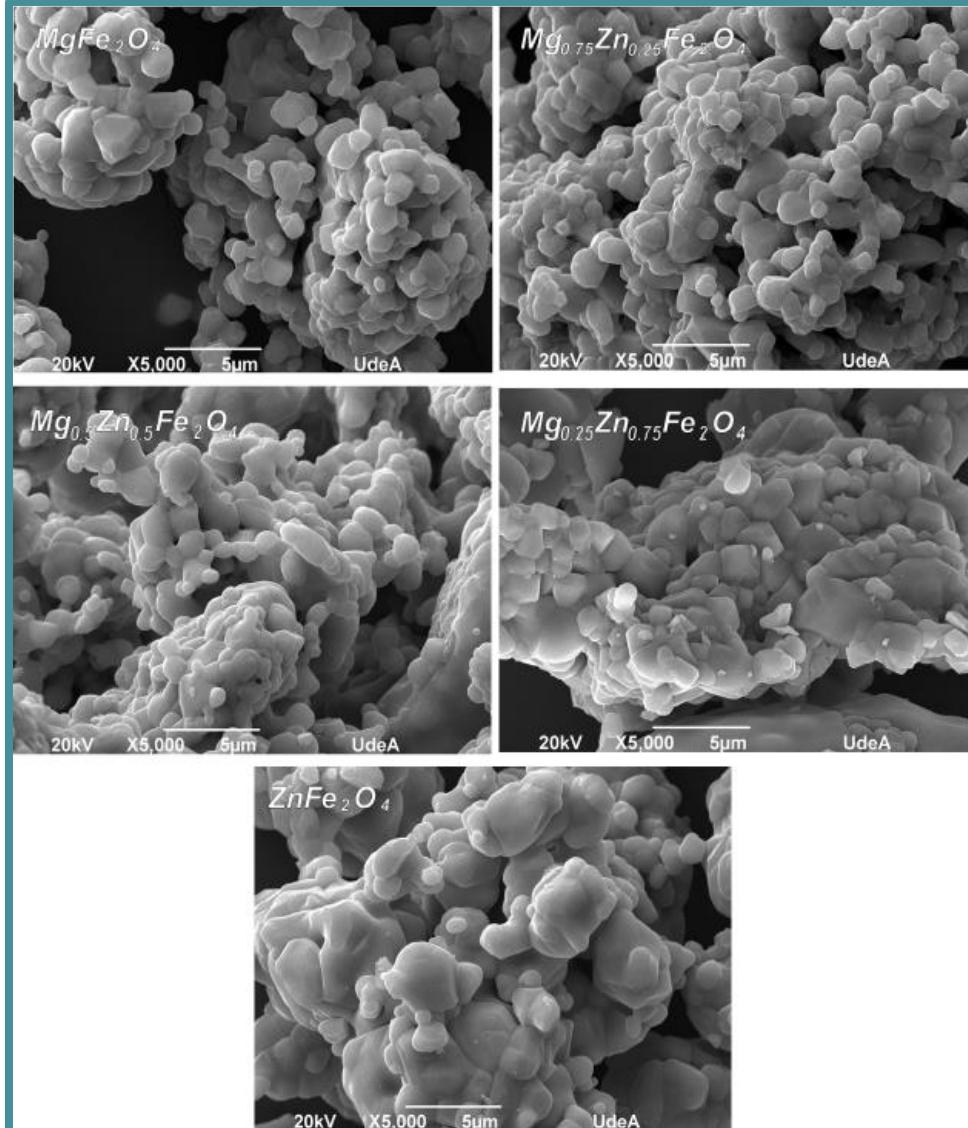
$Zn_xMg_{1-x}Fe_2O_4$	Cation distributions
0.0	$(Mg_{0.11}Fe_{0.89})_A[Mg_{0.89}Fe_{1.11}]_B O_4$
0.25	$(Zn_{0.25}Mg_{0.263}Fe_{0.487})_A[Mg_{0.487}Fe_{1.513}]_B O_4$
0.5	$(Zn_{0.5}Mg_{0.254}Fe_{0.246})_A[Mg_{0.246}Fe_{1.754}]_B O_4$
0.75	$(Zn_{0.75}Mg_{0.114}Fe_{0.136})_A[Mg_{0.136}Fe_{1.864}]_B O_4$
1.0	$(Zn)_A[Fe_2]_B O_4$

Scanning Electron Microscopy (SEM)

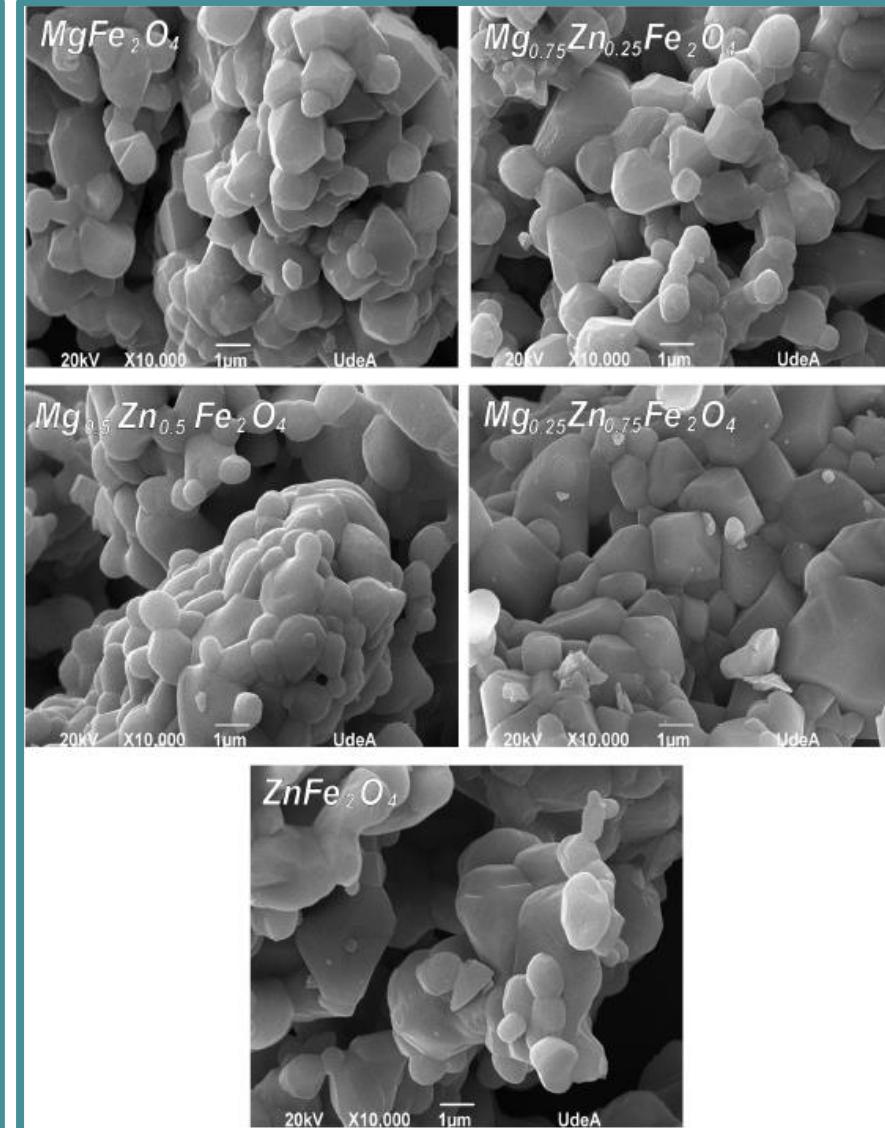
SEM micrograph for the initial reactants mix at 5000x and 40000x magnifications.



SEM micrograph of the mixed ferrites $Zn_xMg_{1-x}Fe_2O_4$ with 5000x magnification.

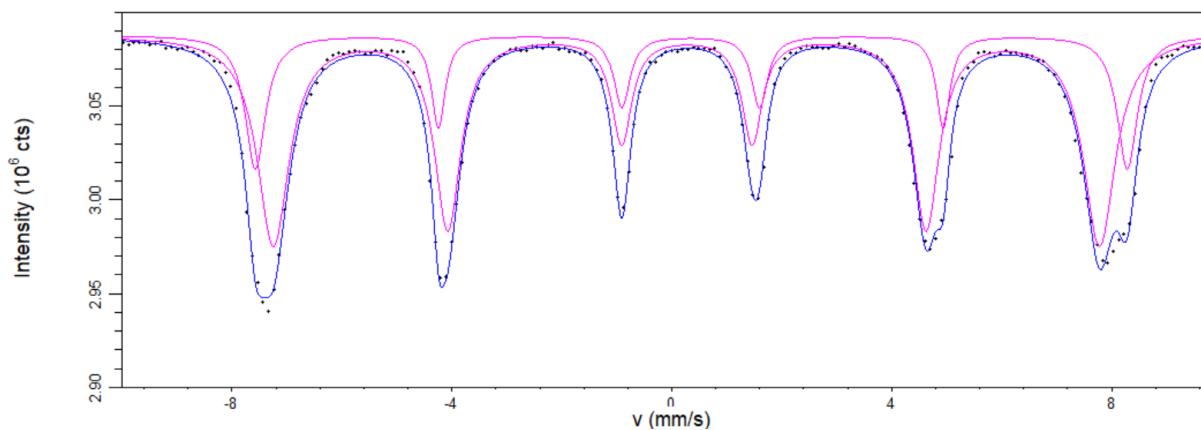


SEM micrograph of the mixed ferrites $Zn_xMg_{1-x}Fe_2O_4$ with 10000x magnification.

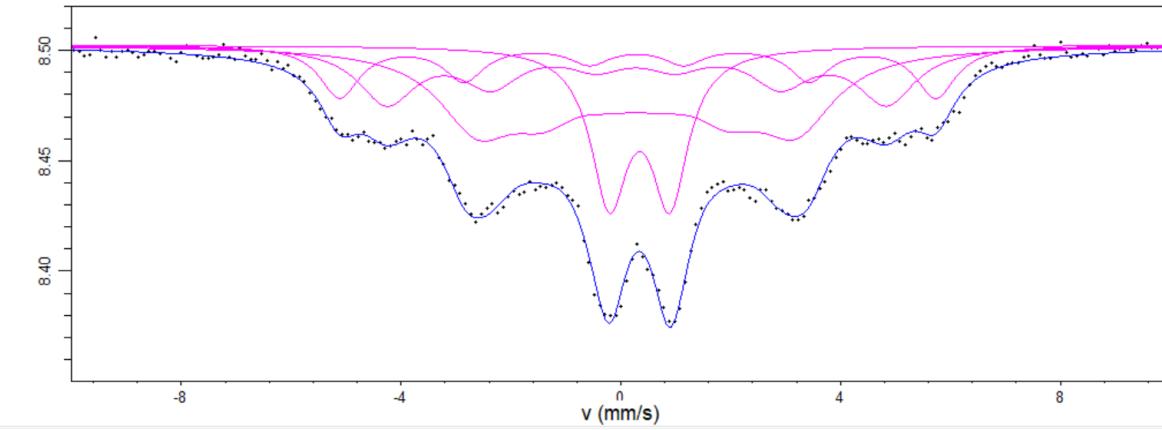


Mössbauer spectra of mixed ferrites $Zn_xMg_{1-x}Fe_2O_4$.

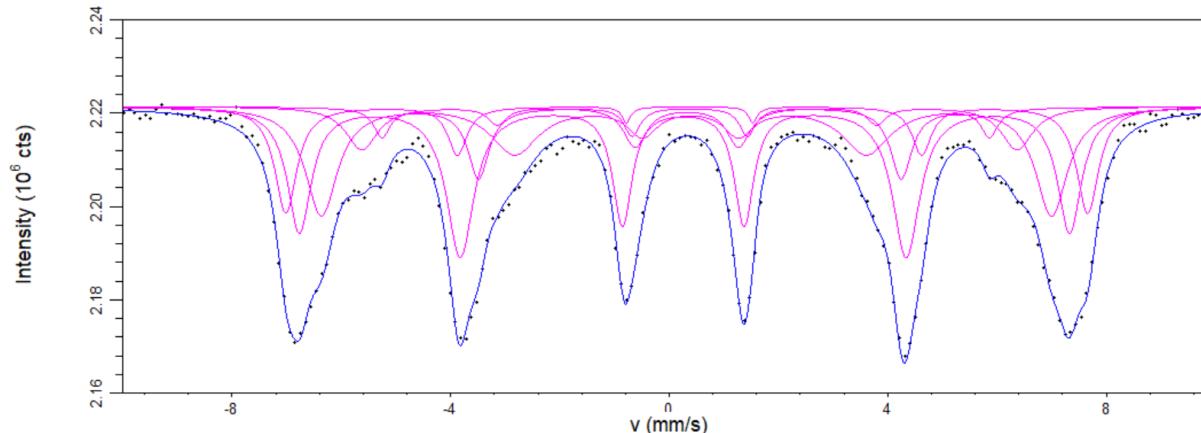
$x = 0$



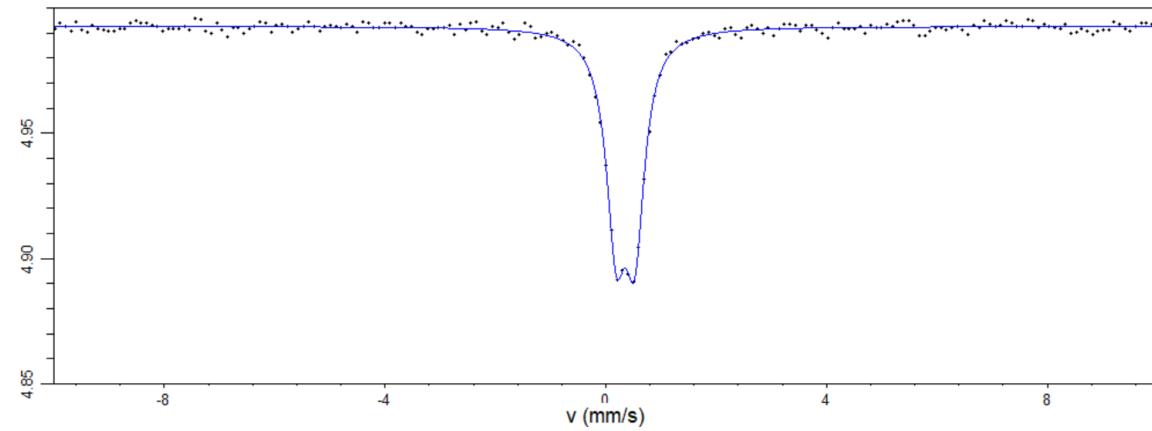
$x = 0.5$

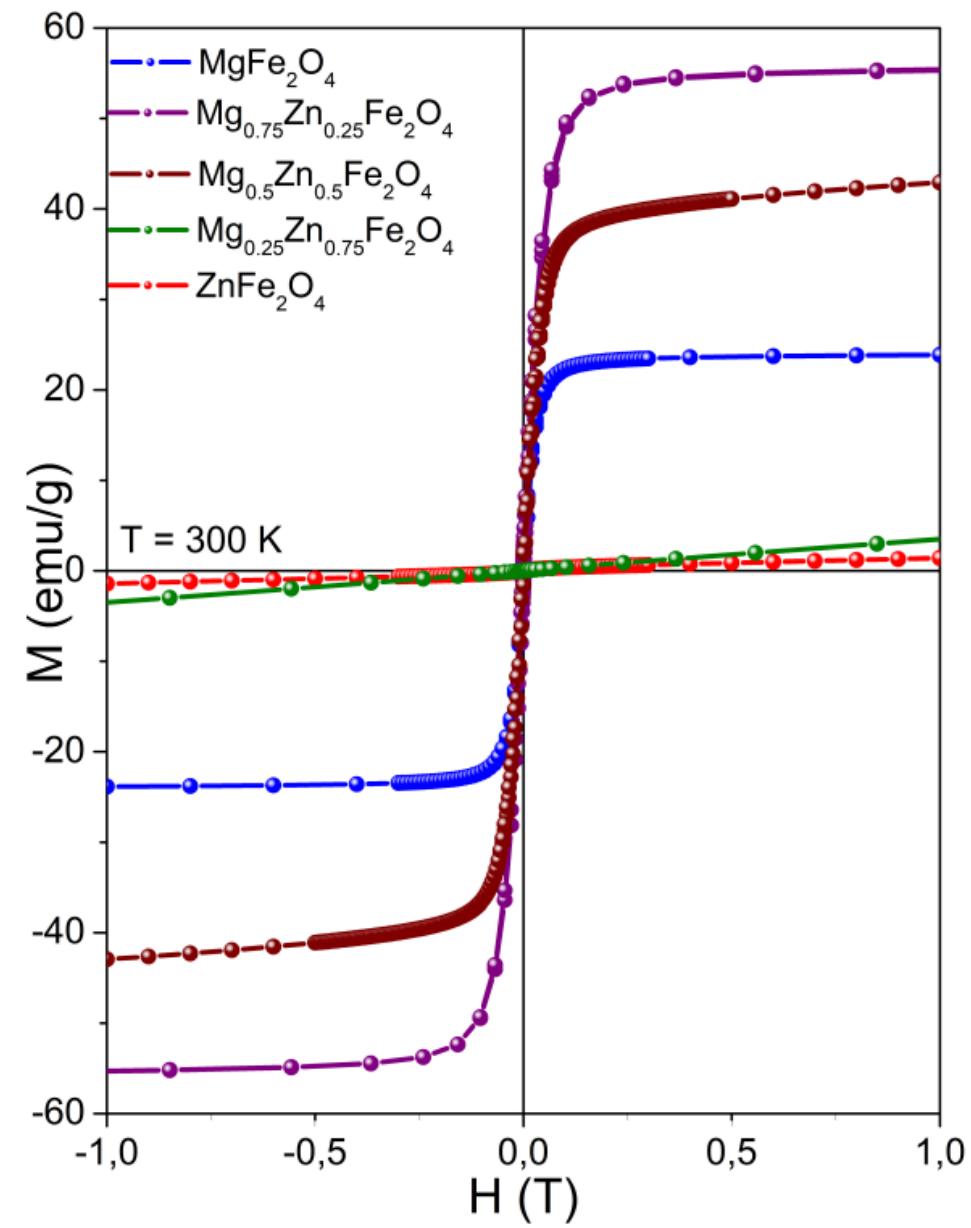
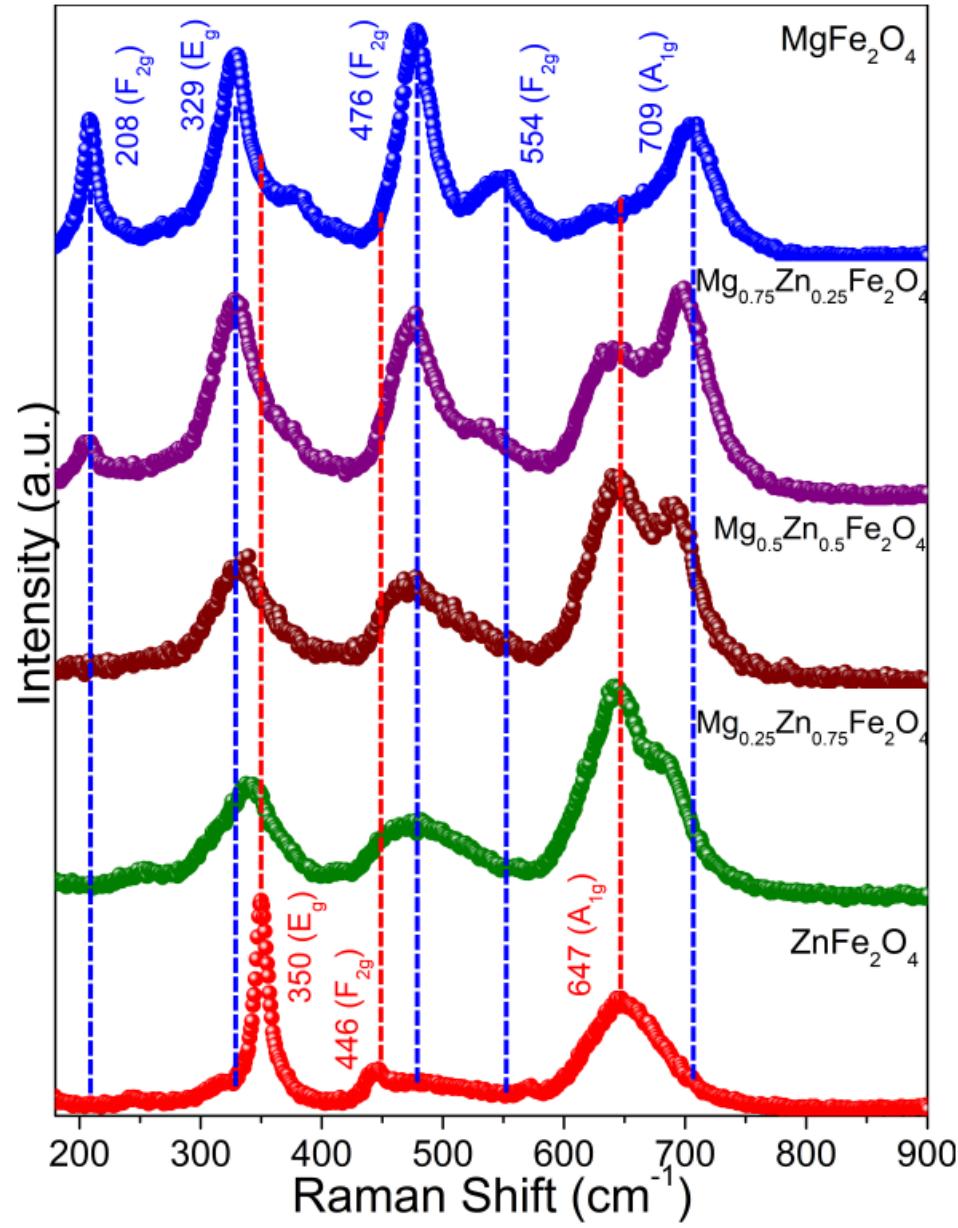


$x = 0.25$



$x = 1$





SUMMARY

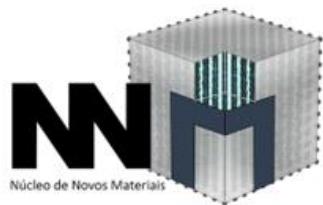
We proposed a simple formula to directly determining the 300 K relative recoilless *f*-factors for the two A and B sites of ferrites. We applied this methodology to three ferrites: NiFe₂O₄, FeFe₂O₄, and MgFe₂O₄. The method can be applied to all ferrites at any temperature.

Defective spinel NiFe₂O₄ is formed at 1000 °C, and as the temperature increases, the defects gradually disappear. Neither cation reordering phenomena nor possible evaporation of chemical elements were the dominant effects to account for the results. The results can be explained if it is assumed that [B]-sites cation vacancies are gradually filled with cations as temperature of heat treatment increases.

The synthesis of the Zn_xM_{1-x}Fe₂O₄ (with M = Ni and Mg) materials and the formation of the spinel structure were confirmed using X-ray diffraction, infrared spectroscopy, scanning electron microscopy and Mössbauer spectroscopy techniques. The presence of Zn²⁺ cations in the tetrahedral site causes a certain amount of Fe³⁺ cations to migrate from site A to site B, which causes important changes in the physico-chemical properties of the samples.

Determination of the stoichiometry of the ferrites were compared by using three different techniques: XRD, Raman and Mössbauer.

iTHANKS!



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